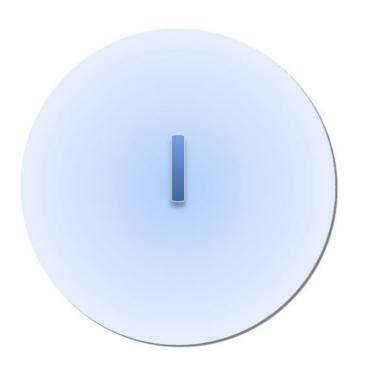
## سلسلة الدوس و المحاضرات

# مدغل الم فيزيا، الصالة الصلبة الجزء اللأول

# موجه إلى طلبة السنة الثالثة فيزاء



المركني بيان المركاط المركاط



بسسم الله الرحمن الرحيم , الحسد لله رب العالمين , والصلاة والسسلام على أشرف المرسلين , وعلى آله وصعبه أجمعين

لقد بين لنا الله من خلال النظام الكوني, استمرادية المواد كأشياء, وتكراد الظواهر كعلاقات سببية, لنراقبها وندركها وننتفع بها في حياتنا بعد أن نقف على حقيقة سلوكها, ونستدل بها على قدرته ووحدانيته, مصداقا لقولته تعالى سنويهم آياتنا في الأفاق وفي أنفسهم حتى بيتبين لهم أنه الحق....(53) سورة فصلت والفيزياء تعد دائبا في مقدمة العلوم المعنية بدراسة المواد والظواهرالطبيعية المختلفة, وهي التي تقود التقدم العلمي والتقني للبشر فنظرة سريعة لما يتم حولنا من إنحازات في مجالات عدة كارتياد الفضاء, و ثورة المعلومات, ونظم الاتصالات, وغيرها كفيلة بإلقاء الضوء على الدور العظيم الذي تضلع به الفيزياء.

وفيزياء الحالة الصلبة موضوع هذا الكتاب هي أحد فروع الفيزياء المعنى بالبعث في طبيعة المواد الصلبة وخصائصها المختلفة: الميكانيكية والكهربية و المغناطيسية والحرارية والضوئية وغيرها.

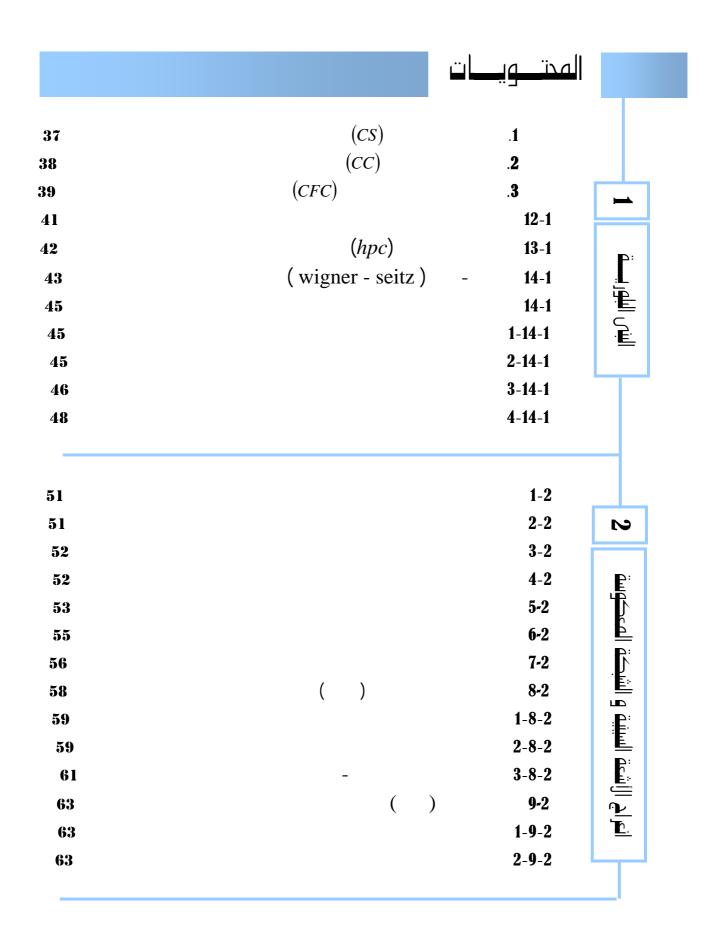
والأجسام الصلبة قد تكون بلورية فتشكل مملكة مترامية الأطراف, رعاياها من المعادن والمواد العازلة و أشباه الموصلات والموصلات الفائقة, وغيرها. وهي تسلك في المظروف المختلفة ضروبا متباينة من السلوك الذي يوحي بمجالات تطبيقية شاسعة. كما أنها قد تكون غيربلورية, ولها هي الأخرى تطبيقاتها الحاصة والكتاب الذي بين أيدينا محاول أن يصعب القارئ العربي في جولة قصية إلى دنيا فيزياء الأجسام الصلبة, حيث اختيرت محتوياته بعناية لكي تلبي احتياجات المقرد الدراسي لمقياس الفيزياء الصلبة في المؤد الشائي وكلاهما خاص بطلاب السنة الثالثة فيزياء P.I.M.D, وقد صيغت خصول هذا الكتاب بشكل مترابط بجعل القارئ لا يجد صعوبة في الفهم و الاسترسال من فصل لآخر.

والله نسأل أن يعيننا على عرض محتويات كتابنا هذا بجزأيه الأول والثاني بالطريقة التي تيسرللقارئ فهمها واستيعابها. ونأمل أن يوجهنا القارئ الكريم إذا ما صادفته هنة أو ملحوظة يرى إضافتها هنا أو هناك .. متمثلين قول القائل:

إن تجر عيبا نسر الخللا جل من لا عيب نيه وعلا

## المحتويات

5				
15			1-1	
15			-	
15			-	
16			2-1	
17			3-1	
18			4-1	
18			1-4-1	
20			2-4-1	
20	(	)	3-4-1	
21			4-4-1	$\perp$
22			5-4-1	<b>—</b>
22			6-4-1	
23			7-4-1	P:
24			5-1	النبس البلوريسة
25			8-1	<u>=</u>
29			9-1	E
30			10-1	Ц,
30			1-10-1	
33		-	2-10-1	
33			3-10-1	
34			4-10-1	
34			5-10-1	
35			6-10-1	
36	(	)	7-10-1	
36	(	)	8-10-1	
37			11-1	



## المحتويات

ယ

الروابط اللورية و الخصائص العرونية

N ( ) 3-9-2 66 انعراج الأشعة السينية والشبكة المعكوسة 4-9-2 68 5-9-2 70 6-9-2 71 7-9-2 74 8-9-2 75 9-9-2 **78** 10-2 80 11-2 83

89	1-3
89	2-3
92	3-3
96	4-3
98	5-3
99	6-3
103	6-3
105	9-3
105	1-9-3
109	2-9-3
111	3-9-3
114	3-9-3

115	5-9-3
118	6-9-3
120	7-9-3
122	7-9-3

1-4 137 2-4 137 3-4 ( ) 139 1-3-4 141 2-3-4 145 4-4 ( ) 147 5-4 154 6-4 159 7-4 162 1-7-4 162

4

اهتزازات الشبكة البلورية و الخصائص العرارية

## لمحتــويـــات

163 - 165 - 168 - 172 2-7-4 173 3-7-4 175 4-7-4 176 178 183

विश्वी पिमबा

البنى البلورية

1-1 مقدمة

أ - المواد الصلبة البلورية

•

**%**99

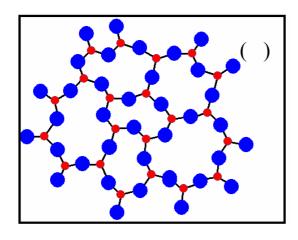
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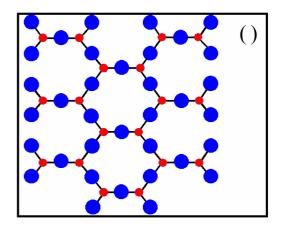
п

. ب- المواد الصلبة اللابلورية

.(1.1)

15





( ) - () : :(1.1)

п

. . .

.

1-2|لشبكة البلورية

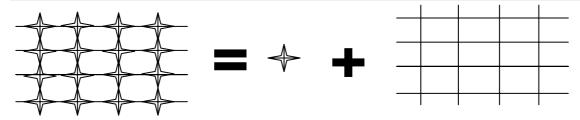
```
1-3 البنية البلورية:
                                                                                                                          (
                                                                                                                         -1
                                                                                                                         -2
                                                                                                                         -3
                                                                                                                         -4
                         ( )
                                           .( )
(
                            .((3.1)
                                   شبكة بلورية + قاعدة (أساس) = بنية بلورية
                                        )\vec{r}'
     (
                                                                                        \vec{r}
(1-1)
                                                     \bar{r}' = \vec{r} + \vec{R}
                                        (
                                                                                         (
                                                                                                  )
(2-1)
                                  \vec{R} = n_1 \vec{a}_1 + n_2 \vec{a}_2 + n_3 \vec{a}_3
                                                                                                          \vec{a}_3 \vec{a}_2 \vec{a}_1:
```

. ((4.1)

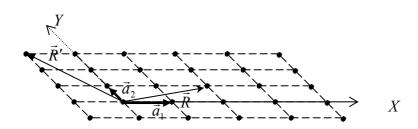
17

 $n_3$   $n_2$   $n_1$ 





:(3.1)



 $\vec{R}' = -\vec{a}_1 + 3\vec{a}_2$   $\vec{R} = 2\vec{a}_1 + \vec{a}_2$ : (4.1)

#### 1-4 التناظر البلوري

( )

1-4-1 التناظر الدوراني

$$\theta = \frac{2\pi}{n}$$

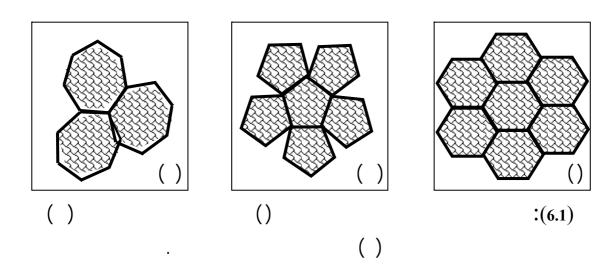
$$n A_n$$
 ((5.1) ) 6.4.3.2.1

 $\vec{R}$ 

البنى البلوس ية

 $\frac{\pi}{3}$   $\frac{\pi}{2}$   $\frac{2\pi}{3}$   $\pi$   $2\pi$ 

 $\begin{array}{c} .(6.1) \\ A_6 \ A_4 \ A_3 \ A_2 \\ \hline \\ 1 \ 2 \ 3 \ 4 \ 6 \\ \hline \\ . \ (5.1) \end{array}$ 

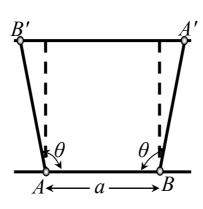


(3-1)  $B'A' = AB(1 + 2\cos(\theta)) = a(1 + 2\cos(\theta))$   $a \qquad A'B' \qquad AB \qquad A'B'$   $\theta \qquad 0 \pm 1 \pm 2 \qquad 2\cos(\theta)$ 

$$\theta = \frac{360^{\circ}}{n}$$

 $.90^{\circ} \ 120^{\circ} \ 60^{\circ} \ 0^{\circ} \ 360^{\circ} \ 180^{\circ}$ 

.

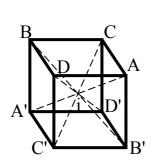


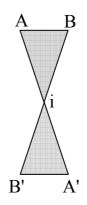
:(7.1)

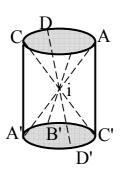
1-4-2 التناظر الانقلابي:

 $\vec{r}$ 

.c (c) . — 
$$-\bar{n}$$







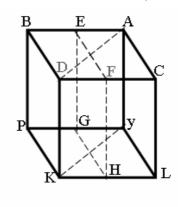
. :(8.1)

1-4-1 التناظر الانعكاسي(المرآتي) وفق مستو:

.m .
)AYKD ADBPYK ACDKYL (9.1)
ACFEGYLH (

البنى البلوس ية

.( )EFHG EFDBPGHK



. :(9.1)

1-4-4 التناظر الدوراني الانقلابي:

C  $A_n$  . n  $\overline{n}$   $\overline{A}_n$ 

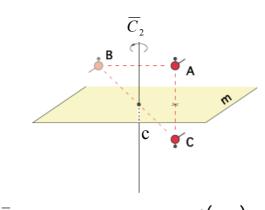
 $\overline{A}_2$  (10.1)

.*m* 

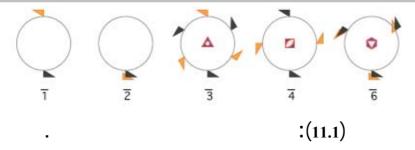
 $\overline{A}_6 \ \overline{A}_4 \ \overline{A}_3 \ \overline{A}_2$ 

c

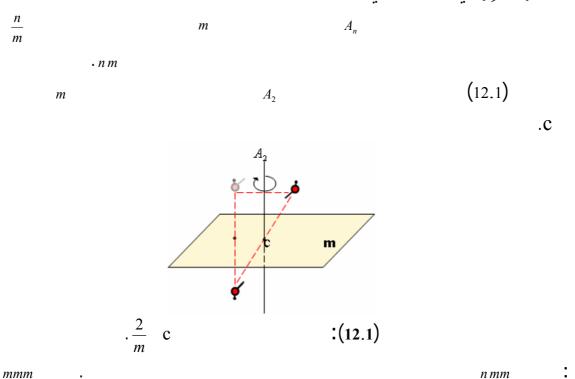
.(11.1) .



 $.\overline{2} m$  :(10.1)



#### 1-4-5 التناظر الدوراني الانعكاسي:



#### 1-4-6 تمثيل عمليات التناظر بالممتدات:

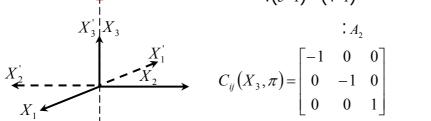
22

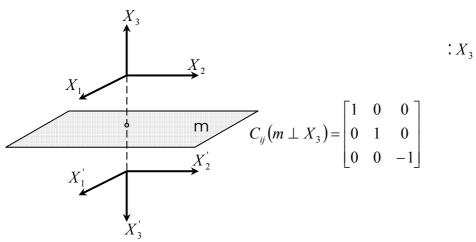
(4-1) 
$$\begin{bmatrix} C_{ij} \end{bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix}$$

(5-1) 
$$C_{ij} = \cos(X_i, X_j)$$

j = 1,2,3 i = 1,2,3 .

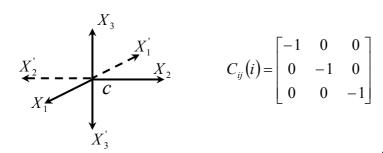
:(5-1) (4-1)





: c .2

.1



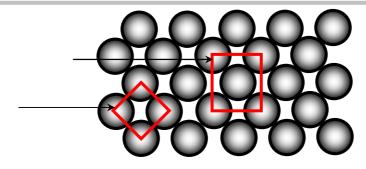
1-4-1 الزمرة النقطية و الزمرة الفضائية:

:

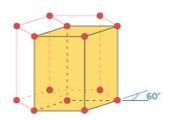
```
. n
                                                                                                                     . m
                                                                                                                                 . i
                                                                                                                                          1-5 خلية الوحدة:
                         \vec{a}_3 \vec{a}_2 \vec{a}_1
(6-1)
                                                                    V_e = \vec{a}.(\vec{b} \times \vec{c})
                                                                                                                                     (13.1)
                               (1+\frac{1}{4}\times 4=2)
                                                                                    \left(\frac{1}{4} \times 4 = 1\right)
                                                                        (14.1)
```

•

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:(13.1)



:(14.1)

8-1 تصنيف الشبكات البلورية الفضائية:

" Bravais"

(( (( )) 230 32 .(2.1) (1.1)

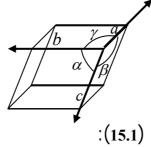
(

(s) .(BC) (C) **(**F**)** )

(

 $\vec{c}$   $\vec{b}$   $\vec{a}$ )  $c \ b \ a$  (c) - (15.1)

 $\boldsymbol{\gamma} = \left(\vec{a}, \vec{b}\right) \quad \boldsymbol{\beta} = \left(\vec{c}, \vec{a}\right) \quad \boldsymbol{\alpha} = \left(\vec{c}, \vec{b}\right) \qquad \boldsymbol{\gamma} \quad \boldsymbol{\beta} \quad \boldsymbol{\alpha} \qquad \left(\vec{a}_3 \quad \vec{a}_2 \quad \vec{a}_1 \right)$ 



 $\alpha \neq \beta \neq \gamma \neq \frac{\pi}{2}$   $a \neq b \neq c$ :

1- الفئة الثلاثية الميل:

 $(c = \overline{1})$ 

 $a \neq b \neq c$ :

2- الفئة أحادية الحيل:

b a

 $-A_{2}$ 

 $\alpha = \gamma = \frac{\pi}{2} \neq \beta$ 

 $\frac{2}{m}$   $\frac{A_2}{m}c$ :

(c)

 $a \neq b \neq c$ :

3- الفئة المعينية المستقيمة:

 $\alpha = \gamma = \beta = \frac{\pi}{2}$ 

 $\frac{2}{m}\frac{2}{m}\frac{2}{m} \qquad \frac{A_2}{m}\frac{A_2}{m}\frac{A_2}{m}c :$ 

(c)

 $a = b \neq c$ :

4- الفئة الرباعية:

 $\alpha = \gamma = \beta = \frac{\pi}{2}$ 

 $A_4$ 

 $\frac{1}{m} \frac{2}{m} \frac{2}{m} \frac{2}{m} \frac{A_4}{m} \frac{2A_2}{2m} \frac{2A_2}{2m} c$ :

(c)

((16.1)

 $\alpha = \gamma = \beta = \frac{\pi}{2}$  a = b = c:

5- الفئة المكعبة:

)  $\frac{4}{m}\bar{3}\frac{2}{m}$   $\frac{3A_4}{m}4A_3\frac{6A_2}{6m}c$ :

。 45 و

((17.1)

a=b=c : : الفئة الثلاثية -6

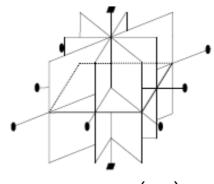
 $- \qquad \qquad \alpha = \gamma = \beta \neq \frac{\pi}{2}$ 

- - A<sub>2</sub>

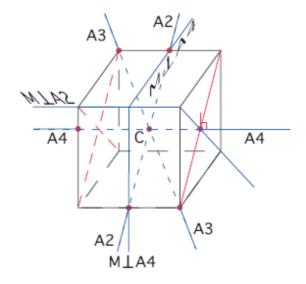
 $\frac{1}{3}\frac{2}{m} A_3 \frac{3A_2}{3m}c$  : (c)

 $\alpha = \gamma = \frac{\pi}{2}, \beta = 120^{\circ}$  a = b = c : : : : : : : -7

 $\frac{6}{m} \frac{2}{m} \frac{2}{m} \frac{2}{m} \frac{A_6}{m} \frac{3A_2}{3m} \frac{3A_2}{3m} c :$ 



:(16.1)



. :(17.1)

	Face centrée	Corps centrée	Base centrée	Simple	
$a \neq b \neq c$ $\alpha \neq \beta \neq \gamma \neq \pi/2$					Triclinique
$a \neq b \neq c$ $\alpha = \gamma = \pi/2 \neq \beta$					Monocliniqu e
$a \neq b \neq c$ $\alpha = \beta = \gamma = \pi/2$					Orthorhombi que
$a = b \neq c$ $\alpha = \beta = \gamma = \pi/2$					Quadratique
$a = b = c$ $\alpha = \beta = \gamma = \pi/2$					Cubique
$a = b = c$ $\alpha = \beta = \gamma$ $\neq \pi/2, <120^{\circ}$					Rhomboédriq ue
$a = b \neq c$ $\alpha = \beta = \pi/2, \gamma = 120^{\circ}$					Hexagonal

:(1.1)

1		с	1	Triclinique
2	$A_2$	$\frac{A_2}{m}c$	$\frac{2}{m}$	Monoclinique
4		$\frac{A_2}{m} \frac{A_2}{m} \frac{A_2}{m} c$	$\frac{2}{m}\frac{2}{m}\frac{2}{m}$	Orthorhombique
2		$\frac{A_4}{m} \frac{2A_2}{2m} \frac{2A_2}{2m} c$ $\frac{3A_4}{m} 4A_3 \frac{6A_2}{6m} c$	$\frac{4}{m}\frac{2}{m}\frac{2}{m}$	Quadratique
3		$\frac{3A_4}{m}4A_3\frac{6A_2}{6m}c$	$\frac{4}{m}\overline{3}\frac{2}{m}$	Cubique
1		$A_3 \frac{3A_2}{3m} c$	$\frac{\bar{3}}{m}$	Rhomboédrique
1		$\frac{A_6}{m} \frac{3A_2}{3m} \frac{3A_2}{3m} c$	$\frac{6}{m}\frac{2}{m}\frac{2}{m}$	Hexagonal

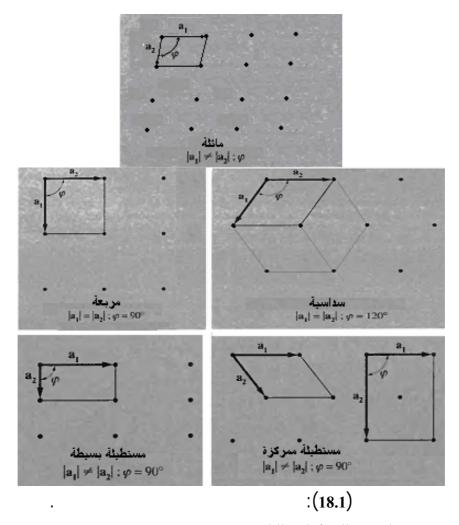
:(2.1)

#### 1-9 تصنيف الشبكات البلورية المستوية:

(c)  $b \ a \qquad \qquad . \varphi = \left(\vec{a}, \vec{b}\right) \qquad \varphi \qquad \qquad b \ a \qquad .$ 

 $\frac{2\pi}{4} \qquad \qquad 2\pi \quad \pi$   $\qquad \qquad \cdot \qquad \qquad \frac{2\pi}{6} \quad \frac{2\pi}{3} \qquad \cdot \qquad \cdot$   $\qquad \qquad \cdot 2mm \qquad \qquad \cdot 4mm \qquad \qquad \cdot$ 

.((16.1) ) 6*mm* 



1-10 التعريف ببعض خصائص الشبكات البلورية:

1-10-1 تحديد مواضع و متجهات المستويات البلورية:

. - -

c,b,a

"Miller "

(X,Y,Z) : •

 $\vec{c}, \vec{b}, \vec{a}$ 

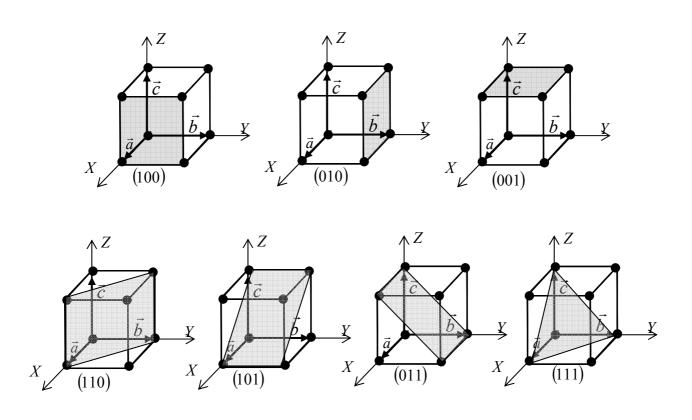
```
البنى البلومرية
```

```
(X,Y,Z)
                                                                                           .c,b,a
                                                                             .(hkl):
                                                                                         (-)
                                                         (19.1)
                                   (X,Y,Z)
               (3a : 2b : 1c)
                                                                         ABC
                                                                (\frac{1}{3}, \frac{1}{2}, 1)
  (\frac{2}{6}, \frac{3}{6}, \frac{6}{6})
                        (6)
                  .(236)
                                   h=2,k=3,l=6
                                                             :(19.1)
                                   .ABC
               . {hkl}
                          (\overline{1}00), (0\overline{1}0), (00\overline{1}), (100), (010), (001)
                                                                                  {001}
(20.1)
           [100]
                       (X)
                                                  \cdot [uvw]
                  :((21.1)
                                                                                          (Y)
                                         ) [001]
                                                    (Z)
                                                                               .[010]
                                                                           \langle uvw \rangle
                                          \langle 110 \rangle
        l = w, k = v, h = u
                                       (hkl)
                                                                [uvw]
```

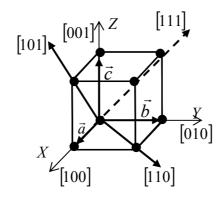
31

.(110) [110] (100)

 $(\frac{1}{2}, \frac{1}{2}, \frac{1}{2})$ : (xyz) .  $(\frac{1}{2}, 0, \frac{1}{2}), (\frac{1}{2}, \frac{1}{2}, 0), (0, \frac{1}{2}, \frac{1}{2})$ :



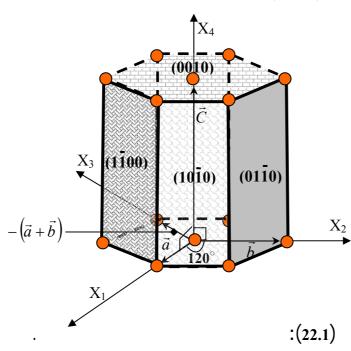
:(20.1)



:(21.1)

#### 1-10-2 قرائن ميلر- برافي للفئة السداسية:

(1/2:1/2:-1:1/3): (2,2,-1,3) (X1,X2,X3,X4).  $(hkil) = (3,3,\overline{6},2)$  6:



#### 1-10-3 المسافة الفاصلة بين المستويات البلورية المتوازية:

 $d_{hkl}$  a  $\vdots \quad a \qquad l, k, h$   $d_{hkl} = \frac{a}{\sqrt{h^2 + k^2 + l^2}}$   $\vdots \quad (111) \quad (110) \quad (100)$ 

33

(8-1) 
$$d_{100} = \frac{a}{\sqrt{1+0+0}} = a$$

{100} .a

(9-1) 
$$d_{110} = \frac{a}{\sqrt{1+1+0}} = \frac{a}{\sqrt{2}} = \frac{a}{1.4}$$

. {100} {110}

(10-1) 
$$d_{111} = \frac{a}{\sqrt{1+1+1}} = \frac{a}{\sqrt{3}} = \frac{a}{1.7}$$
 {111}

ملاحظة:  $d_{hkl}$ 

#### 1-10-4 كثافة المستويات البلورية:

(hkl)

: .  $\sigma_{hkl}$ 

(11-1) 
$$\sigma_{hkl} = \sum_{i} \frac{n_{hkl}^{i} S_{a}^{i}}{S_{hkl}}$$

$$(hkl) : S_{hkl}, i : S_a^i, (hkl) i : n_{hkl}^i:$$

#### 1-10-5 معادلة مستوي بلوري:

$$D, C, B, A Ax + By + Cz = D :$$

$$(23.1) p_3(0,0,\frac{a_3}{l}) p_2(0,\frac{a_2}{k},0) p_1(\frac{a_1}{h},0,0)$$

$$\vdots (hbl)$$

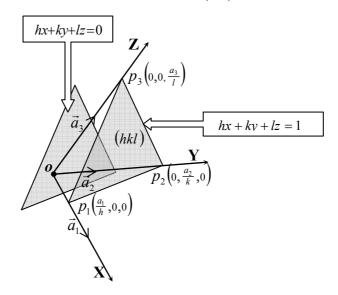
$$\begin{cases}
A \times \frac{a_1}{h} = D \\
B \times \frac{a_2}{k} = D \\
C \times \frac{a_3}{l} = D
\end{cases} \Rightarrow
\begin{cases}
A = \frac{h}{a_1} D \\
B = \frac{k}{a_2} D \\
C = \frac{l}{a_3} D
\end{cases} \Rightarrow \frac{h}{a_1} D x + \frac{k}{a_2} D y + \frac{l}{a_3} D z = D \Rightarrow$$

(12-1) 
$$\frac{h}{a_1}x + \frac{k}{a_2}y + \frac{l}{a_3}z = 1$$

: 
$$(12-1)$$
  $a_3, a_2, a_1$   $z, y, x$ 

$$(13-1) hx + ky + lz = 1$$

. (hkl) (13-1)



$$hx + ky + lz = 0$$
  $hx + ky + lz = 1$  :(23.1)

(hkl)

$$(14-1) hx + ky + lz = m$$

 $(m = 0, \pm 1, \pm 2....)$  : m

.((23.1) ) 
$$(m = \pm 1)$$

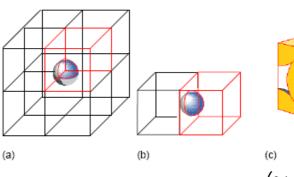
 $n_a$  عدد عقد خلية الوحدة 6-10-1

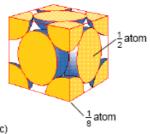
$$(24.1)$$
 : . ( )

 $\left(1 = 8 \times \frac{1}{8}\right) :$ 

$$\left(4 = 3 + 1 = 3 \times \frac{1}{2} + 8 \times \frac{1}{8}\right)$$
:  $\left(3 = 6 \times \frac{1}{2}\right)$ :

.





:(24.1)

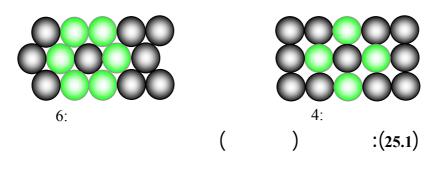
البنى البلوسية

#### 1-10-1 عدد الجوار الأول(عدد التناسق) Z:

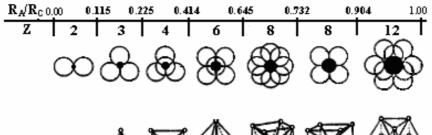
( ) .(25.1)

 $R_{Z}$ 

:\_\_



 $.R_A/R_C$  ( / ) ( / )





 $R_A/R_C$  :(26.1)

 $: F_{R}$  (الرص) عامل التعبئة (الرص\*8 -10-1

(26.1)

: .

$$F_R = \sum_i \frac{n_a^i v_a^i}{V}$$

:

 $\vdots V . i \qquad \vdots V_a^i . \qquad i \qquad \vdots n_a^i$ 

 $m_i$   $v_i$  (15-1)  $\rho$ 

.

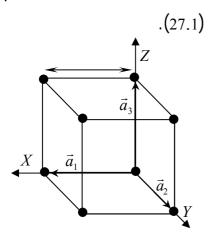
(16-1) 
$$\rho = \sum_{i} \frac{n_a^i m_a^i}{V}$$

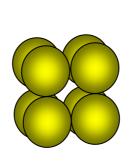
1-11 دراسة شبكات الفئة المكعبة:

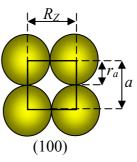
:

1. الشبكة المكعبة البسيطة (CS)

( )







:(27.1)

- خصائص الشبكة المكعبة البسيطة:

$$\vec{a}_1 = a\vec{i}, \vec{a}_2 = a\vec{j}, \vec{a}_1 = a\vec{k}$$
 : .1

$$\vec{R} = n_1 \vec{a}_1 + n_2 \vec{a}_2 + n_3 \vec{a}_3 = n_1 a \vec{i} + n_2 a \vec{j} + n_3 a \vec{k} \quad .$$

$$V_e = \vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3) = a\vec{i} \cdot (a\vec{j} \times a\vec{k}) = a^3$$
:

$$n_a = \frac{1}{8} \times 8 = 1 \ :$$

$$z = 6$$
: .5

$$: r_a: \qquad R_z = 2r_a = a : \qquad . \mathbf{6}$$

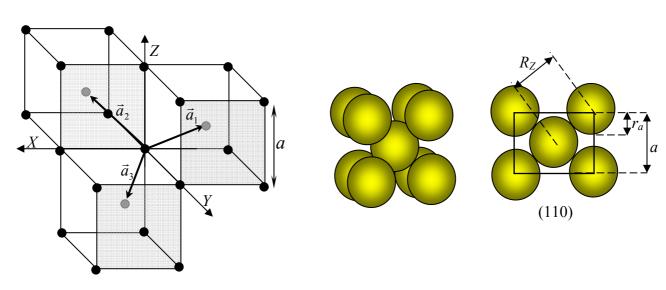
$$F_R^{CS} = \frac{n_a v_a}{V} = \frac{1 \times \frac{4}{3} \pi r_a^3}{a^3} = \frac{\frac{4}{3} \pi (\frac{a}{2})^3}{a^3} = \frac{\pi}{6} = 0.52$$
:

البني البلوم به

$$\sigma_{hkl} = \frac{n_{hkl} s_a}{s_{hkl}} = \frac{\left(4 \times \frac{1}{4}\right) \pi r_a^2}{a^2} = \frac{\pi \left(\frac{a}{2}\right)^2}{a^2} = \frac{\pi}{4} = 0.78 \ \ \{100\}$$

2. الشبكة المكعبة الممركزة (CC).

.(27.1)



:(28.1)

- خصائص الشبكة المكعبة الممركزة:

$$\vec{a}_3 = \frac{a}{2} (\vec{i} + \vec{j} - \vec{k}) \quad \vec{a}_2 = \frac{a}{2} (\vec{i} - \vec{j} + \vec{k}) \quad \vec{a}_1 = \frac{a}{2} (-\vec{i} + \vec{j} + \vec{k}) :$$

: **.2** 

$$a_1 = a_2 = a_3 = \frac{\sqrt{3}}{2}a$$
,  $\gamma = \beta = \alpha = \arccos\left(\frac{\vec{a}_1 \cdot \vec{a}_2}{\|\vec{a}_1\| \cdot \|\vec{a}_{21}\|}\right) = \arccos\left(-\frac{1}{3}\right) = 109.47^{\circ}$ 

**.3** 

 $\vec{R} = n_1 \vec{a}_1 + n_2 \vec{a}_2 + n_3 \vec{a}_3 = \frac{a}{2} \left( \left( -n_1 + n_2 + n_3 \right) \vec{i} + \left( n - n_2 + n_3 \right) \vec{j} + \left( n_1 + n_2 - n_3 \right) \vec{k} \right)$ 

$$V_e = \vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3) = a^3 / 2$$
:

$$.\left(\frac{1}{2}, \frac{1}{2}, \frac{1}{2}\right) (0,0,0) n_a = \frac{1}{8} \times 8 + 1 = 2 .5$$

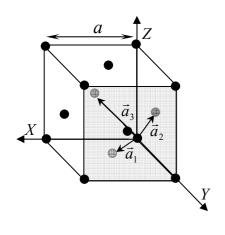
z = 8: .6

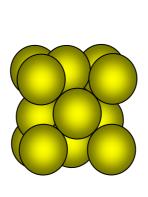
: 
$$r_a$$
:  $R_z = 2r_a = \sqrt{\left(\frac{a}{2}\right)^2 + \left(\frac{a}{2}\right)^2 + \left(\frac{a}{2}\right)^2} = \frac{\sqrt{3}}{2}a$ : .7

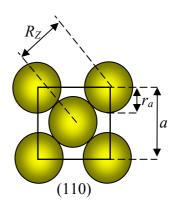
$$F_R^{CC} = \frac{n_a v_a}{V} = \frac{2 \times \frac{4}{3} \pi r_a^3}{a^3} = \frac{\frac{8}{3} \pi \left(\frac{\sqrt{3}}{4} a\right)^3}{a^3} = \frac{\pi \sqrt{3}}{8} = 0.68$$
:

3. الشبكة المكعبة الممركزة الأوجه (CFC).

. (29.1)







:(29.1)

- خصائص الشبكة المكعبة الممركزة الأوجه:

$$\vec{a}_3 = \frac{a}{2}(\vec{i} + \vec{j}) \quad \vec{a}_2 = \frac{a}{2}(\vec{i} + \vec{k}) \quad \vec{a}_1 = \frac{a}{2}(\vec{j} + \vec{k}) :$$
 .1

: **.2** 

$$a_1 = a_2 = a_3 = \frac{\sqrt{2}}{2} a$$
,  $\gamma = \beta = \alpha = \arccos\left(\frac{\vec{a}_1 \cdot \vec{a}_2}{\|\vec{a}_1\| \cdot \|\vec{a}_{21}\|}\right) = \arccos\left(\frac{1}{2}\right) = 60^{\circ}$ 

3. شعاع الانسحاب الأساسي:

$$\vec{R} = n_1 \vec{a}_1 + n_2 \vec{a}_2 + n_3 \vec{a}_3 = \frac{a}{2} ((n_2 + n_3)\vec{i} + (n_1 + n_3)\vec{j} + (n_1 + n_2)\vec{k})$$

$$V_e = \vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3) = a_4^3 / 4$$
:

$$\left(\frac{1}{2},0,\frac{1}{2}\right)\left(0,\frac{1}{2},\frac{1}{2}\right)$$
 (0,0,0)  $n_a = \frac{1}{8} \times 8 + \frac{1}{2} \times 6 = 4$ :

 $\cdot \left(\frac{1}{2}, \frac{1}{2}, 0\right)$ 

$$z = 12$$
: .6

$$: r_a: R_z = 2r_a = \sqrt{\left(\frac{a}{2}\right)^2 + \left(\frac{a}{2}\right)^2} = \frac{\sqrt{2}}{2}a: .7$$

$$F_R^{CFC} = \frac{n_a v_a}{V} = \frac{4 \times \frac{4}{3} \pi r_a^3}{a^3} = \frac{\frac{16}{3} \pi \left(\frac{\sqrt{3}}{4} a\right)^3}{a^3} = \frac{\pi \sqrt{2}}{6} = 0.74 :$$
 .8

9. المستويات الأكثر كثافة هي المستويات (111):

$$\sigma_{hkl} = \frac{n_{hkl} s_a}{s_{hkl}} = \frac{\left(4 \times \frac{1}{4} + 1\right) \pi r_a^2}{\frac{\sqrt{3}a^2}{2}} = \frac{4\pi \left(\frac{\sqrt{2}}{4}a\right)^2}{\sqrt{3}a^2} = \frac{\pi}{2\sqrt{3}} = 0.9$$

		_			
(CFC)	(CC)	(CS)			
$a^3$	$a^3$	$a^3$	. (	: a)	*
4	2	1	•		*
$\frac{4}{a^3}$	$\frac{2}{a^3}$	$\frac{1}{a^3}$			*
12	8	6			*
$a\sqrt{2}/2$	$a\sqrt{3}/2$	а			*
6	6	12			*
a	a	$a\sqrt{2}$			*
{111}	{110}	{100}			*

:(3.1)

(4.1)

البنى البلومرية

(CFC)		(CC)		(CS)		
a(Å)		a(A)		a(A)		
3.15	Мо	5.26	Ar			
2.87	Fe	4.5	Al			
5.2	Ва	5.58	Са			
3.31	Та	5.30	Ac			
3.2	V	4.95	Pb			
3.16	W	3.92	Pt	(α)	Po	

. :(4.1)

#### 12-1 التعبئة المتراصة:

( ) A .

В

.A B

·

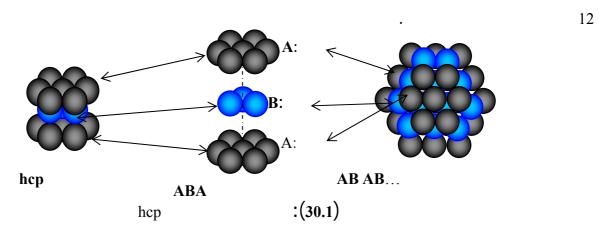
C ) A B C AB AB... (30.1) (A

. 12 (hcp)

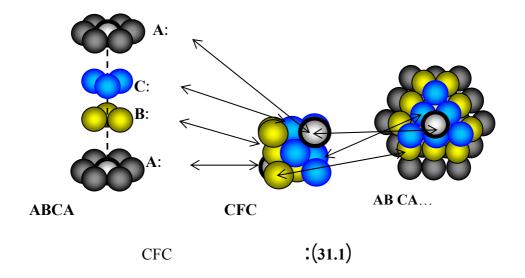
A B C :

(31.1) A D

(CFC) ABC ABC...



41

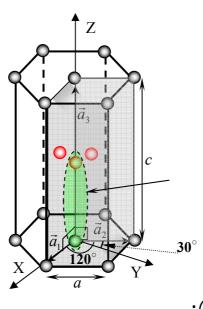


#### 1-13 الشبكة السداسية المتراصة (npc):

 $(32.1) \qquad (\frac{2}{3}, \frac{1}{3}, \frac{1}{2}) \quad (0,0,0)$ 

 $\left(\frac{2}{3},\frac{1}{3},\frac{1}{2}\right)$ :

 $\left(\frac{2}{3}, \frac{1}{3}, \frac{1}{2}\right) \left(\frac{2}{3}, \frac{1}{3}, \frac{1}{2}\right)$ 



. :(32.1)

البنى البلوسرية

خصائص الشبكة السداسية المتراصة (hcp)

$$\vec{a}_1 = a\vec{i}, \vec{a}_2 = \frac{\sqrt{3}}{2}a\vec{j} - \frac{1}{2}a\vec{i}, \vec{a}_1 = c\vec{k}$$
:

: .**2** 

$$a_1 = a_2 = a$$
,  $a_3 = c$ ,  $\beta = \alpha = 90^\circ$ ,  $\gamma = 120^\circ$ 

$$\vec{R} = n_1 \vec{a}_1 + n_2 \vec{a}_2 + n_3 \vec{a}_3 = n_1 \frac{a}{2} (2n_1 - n_2) \vec{i} + \frac{\sqrt{3}}{2} n_2 a \vec{j} + n_3 c \vec{k} \quad :$$

$$\frac{c}{a} = \sqrt{\frac{8}{3}} = 1.63 : \qquad : \frac{c}{a} \qquad .4$$

$$V_e = \vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3) = \frac{\sqrt{3}}{2} a^2 c = \sqrt{2} a^3$$
:

$$\frac{3\sqrt{3}}{2}a^2c = 3\sqrt{2}a^3$$
:

2: 
$$n_a = \frac{1}{6} \times 12 + \frac{1}{2} \times 2 + 3 = 6$$
 : .6

$$z = 12$$
: .7

$$: r_a: \qquad R_z = 2r_a = a : \qquad .8$$

$$F_R^{hcp} = \frac{n_a v_a}{V} = \frac{6 \times \frac{4}{3} \pi r_a^3}{3\sqrt{2} a^3} = \frac{\pi \sqrt{2}}{6} = 0.74 : \tag{5.1}$$

hcp:							
c(A)	a(A)		c(A)	$a(\stackrel{\circ}{\mathrm{A}})$			
6.07	3.75	La	3.58	2.29	Ве		
5.21	3.21	Mg	5.62	2.98	Cd		
5.27	3.31	Sc	5.59	3.56	Er		
5.73	3.65	Y	5.78	3.64	Gd		
5.69	3.60	Tb	5.83	3.57	Не		
4.95	2.66	Zn	5.62	3.58	Но		

:(5.1)

14-1 خلية ويغنر - زايتس ( wigner - seitz ):

.1

البنى البلومرية

.((33.1) ) .2

( ) .3

- :(33.1) CFC - (34.1)

- . CFC ( ) CC

.CC

(→) CC

(i) CFC

- :(34.1)

البنى البلومرية

#### 1-14 بعض البني البلورية المشهورة:

#### 1-14-1 بنية الماس:

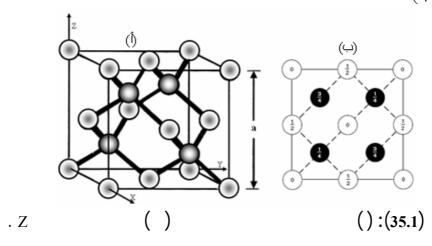
$$\left(\frac{1}{4}, \frac{1}{4}, \frac{1}{4}\right) (0,0,0)$$
:

$$(z = 4)$$

$$(z = 4)$$

$$\left(\frac{1}{4}, \frac{3}{4}, \frac{3}{4}\right) \left(\frac{1}{4}, \frac{1}{4}, \frac{1}{4}\right) \left(\frac{1}{2}, \frac{1}{2}, 0\right) \left(\frac{1}{2}, 0, \frac{1}{2}\right) \left(0, \frac{1}{2}, \frac{1}{2}\right) \quad (0, 0, 0)$$

$$\cdot \left(\frac{3}{4}, \frac{3}{4}, \frac{1}{4}\right) \left(\frac{3}{4}, \frac{1}{4}, \frac{3}{4}\right)$$



$$(F = 0.34)$$
 % 34

Z (X,Y)

(35.1)

.Z

2-14-1 بنية كلوريد السيزيوم CsCl:

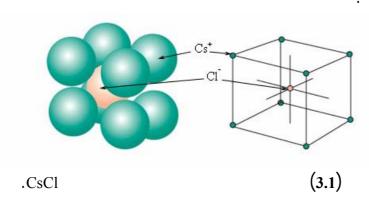
,

$$.\left(\frac{1}{2},\frac{1}{2},\frac{1}{2}\right) \qquad \qquad \text{Cl}^{-} \qquad \qquad \left(0,0,0\right) \qquad \qquad \text{Cs}^{+}$$

CsCl

البنى البلوم ية

(z=8)  $Cl^{-} Cs^{+}$   $R_{z} = r_{Cl^{-}} + r_{Cs^{+}} = \frac{\sqrt{3}}{2}a$ 



3-14-1 بنية كلوريد الصوديوم NaCl:

( )

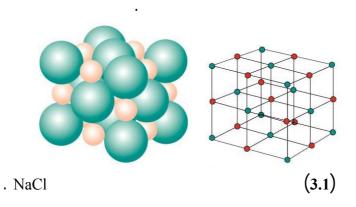
$$.\left(\frac{1}{2},0,0\right)$$
 (C1<sup>-</sup>) (0,0,0) (Na<sup>+</sup>) (C1<sup>-</sup>)

NaCl

$$\cdot \left(0,0,\frac{1}{2}\right) \left(0,\frac{1}{2},0\right) \left(\frac{1}{2},0,0\right) \left(\frac{1}{2},\frac{1}{2},\frac{1}{2}\right) : Na^{+} \left(\frac{1}{2},\frac{1}{2},0\right) \left(\frac{1}{2},0,\frac{1}{2}\right) \left(0,\frac{1}{2},\frac{1}{2}\right) \quad (0,0,0) : Cl^{-}$$

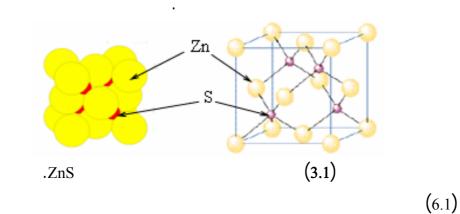
$$\left(z = 6\right) \qquad \qquad Cl^{-} \quad Na^{+}$$

 $R_z = r_{Cl^-} + r_{Na^+} = \frac{a}{2}$ 



لبنى البلومرية

# 1-14-1 بنية كبريت الزنك ZnS:



ZnS		NaCl		CsCl			
a(A)		a(A)		$a(\overset{\circ}{\mathrm{A}})$		$a(\overset{\circ}{\mathrm{A}})$	
5.41	ZnS	5.64	NaCl	4.12	CsCl	3.57	C
6.09	ZnTe	5.35	KF	4.29	CsBr	5.43	Si
5.82	CdS	5.91	CaSe	4.57	CsI	5.66	Ge
6.08	HgSe	5.55	AgCl	3.83	TlCl	6.49	$(\alpha)$ -Sn
5.62	AlSb	4.21	MgO	3.97	TlBr		

:(6.1)

لفصل الثانين

# انعراج الأشعةالسينية والشبكة المعكوسة

2-1 مقدمة:

( - )

P

h

λ

 $\lambda = \frac{h}{p}$ 

 $\vec{a}, \vec{b}, \vec{c}$ 

.

2-2 انعراج النيترونات:

(p) (1-2)

:

(2-2) 
$$E_{n} = \frac{p^{2}}{2m} = \frac{h^{2}}{2m_{n}\lambda_{n}^{2}} \implies \lambda_{n} = \frac{h}{\sqrt{2m_{n}E_{n}}}$$
$$(m_{n}=1.675\times10^{-27} \, Kg) \qquad (2-2)$$

:

(3-2) 
$$\lambda_n \approx \frac{0.28}{\sqrt{E_n}} \stackrel{o}{A}$$

51

 $(E_n = 0.08 \ ev)$ 

0.025 ev

KT

. 4000 m/s

3-2 انعراج الإلكترونات:

**(**2-2**)** 

:  $(m_e = 9.1 \times 10^{-31} Kg)$  $\lambda_e = \frac{12.25}{\sqrt{E_e}} \stackrel{o}{\rm A}$ (4-2)

. 150 ev

2-4 الأشعة السينية المستعملة في تحليل البنية البلورية:

 $\cdot \left(1 \rightarrow 10 \stackrel{o}{A}\right) \qquad - \qquad -$ 

(5-2) 
$$E = \hbar \omega = h \upsilon = h \frac{c}{\lambda} \Rightarrow \lambda = \frac{hc}{E}$$

, hc = 1240 ev.nm

(5-2)  $\left(1 \stackrel{\circ}{A} = 10^{-10} m\right)$  $(1ev = 1.602 \times 10^{-19})$  (Kev)

 $\lambda = \frac{1240 \ [ev.nm]}{E \ [Kev]} = \frac{12.4}{E} \stackrel{o}{A}$ (6-2)

(10-50Kev)

5-2 إنتلج الأشعة السينية:

((1.2)

((2.2)

. ((3.2)

(

 $\gamma \quad \beta \quad \alpha$ 

γ β ,1 3 2

 $.\mathsf{K}_{\alpha}$ Κ M

 $.K_{\beta}$ K

L

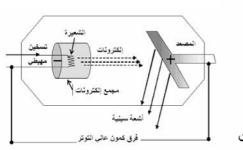
(1.2)

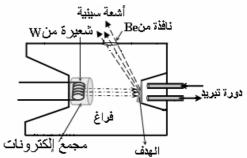
W

**53** 

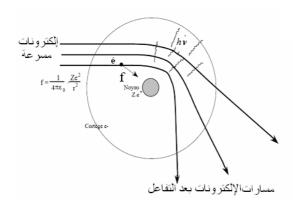
Ве

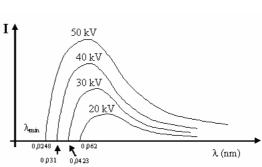
.



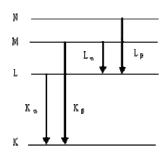


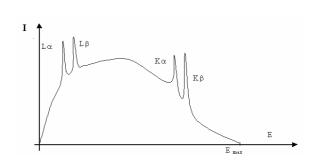
:(1.2)





:(2.2)





:(3.2)

**(**7-2**)** 

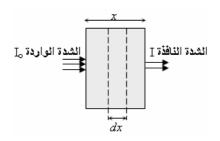
# 6-2 إمتصاص الأشعة السينية:

$$\mu \qquad \qquad (I_o) \qquad \qquad .(\lambda)$$

$$:((4.2) \qquad ) \qquad (I)$$

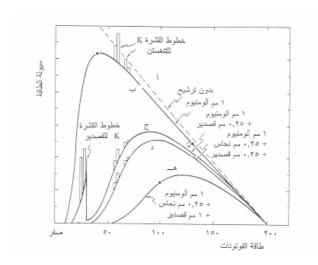
$$I - I_o = dI = -\mu I dx \Rightarrow \int_{I_o}^{I} \frac{dI}{I} = \int_{0}^{x} \mu dx \Rightarrow I = I_o e^{-\mu x}$$

: *x* :



:(4.2)

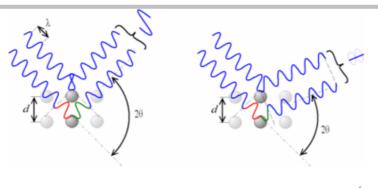
. ((5.2)



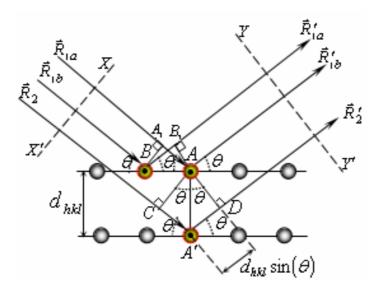
. :(5.2)

# 7-2 علاقة براغ في انعرلج الأشعة السينية :

1913 ((5.2) ((6.2)



:(6.2)



:(7.2)

B A  $\vec{R}_{1b}$   $\vec{R}_{1a}$ 

 $\vec{R}'_{1a}$  YY' XX'

 $\vec{R}'_{{\scriptscriptstyle 1}b}$ 

(8-2) 
$$AA_{1} - BB_{1} = AB\cos(\theta) - AB\cos(\theta) = 0$$

$$\vec{R}'_{1a}$$

•

 $\vec{R}'_{2} \quad \vec{R}'_{1a} \qquad (7.2)$   $\vec{R}'_{2} \quad \vec{R}'_{1a} \qquad (CA' + A'D) : \quad YY' \quad XX' \qquad A'$ 

 $CA' + A'D = 2CA' = n\lambda$  $\sin(\theta) = \frac{CA'}{d_{hkl}} \Rightarrow CA' = d_{hkl} \sin(\theta)$ 

 $2CA' = 2d_{hkl} \sin(\theta) = n\lambda$ 

 $(9-2) 2d_{hkl} \sin(\theta) = n\lambda$ 

 $:\lambda$  ,  $:\theta$  , n:

 $d_{hkl} (9-2)$ 

. n

8-2 الطرق التجريبية لانعراج الأشعة (الأمواج) السينية على البلورات:

 $(2d\sin\theta = n\lambda)$   $(\lambda) \qquad (\lambda) \qquad (\theta)$ 

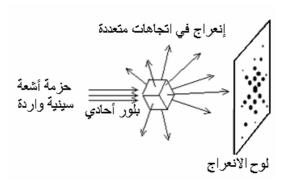
( heta)

 $\{hkl\}$ 

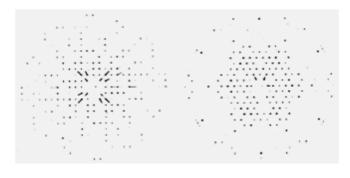
.

# 2-8-1 طريقة فون لاوي (**von Laue**):

 $\begin{pmatrix}
0.2 - 3 \stackrel{\circ}{A} \\
 & (\theta) \\
 & (\lambda) \\
 & (d_{hkl}) \\
 & \vdots \\
 & \vdots \\
 & (9.2) \\
 & )( )$ 



:(8.2)



:(9.2)

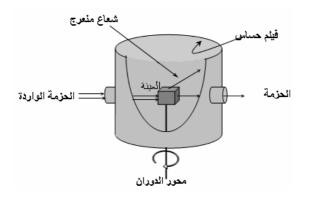
#### 2-8-2 طريفة البلورة الدوارة:

 $(\theta)$ 

 $(d_{hkl})$ 

)

.((10.2)

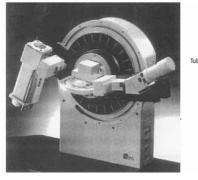


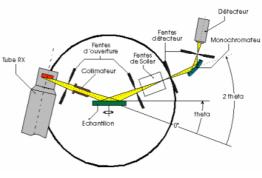
. :(10.2)

) "

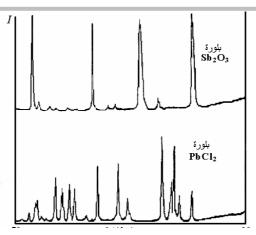
(12.2) .((11.2)

 $.PbCl_2 \quad Sb_2O_3 \\$ 





. :(11.2)



.  $PbCl_2$   $Sb_2O_3$  :(12.2)

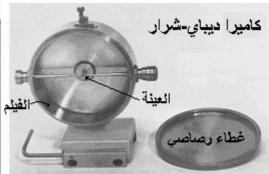
3-8-2 طريقة المسحوق أو طريقة ديباي- شرر Debye-scherrer

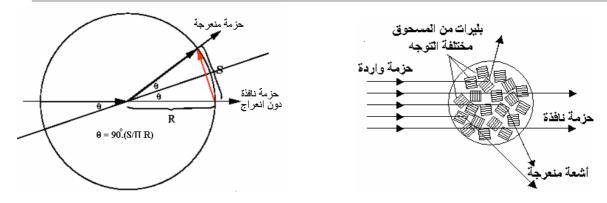
( ) .  $(\theta)$ 

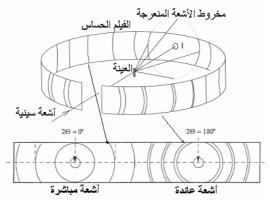
.((13.2) )

.(12.2)



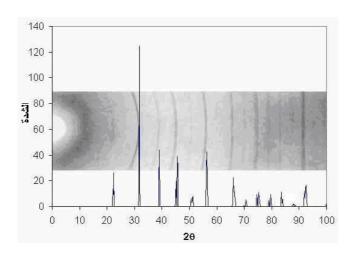






:(13.2)

(14.2)



:(14.2)

2

9-2 الشبكة المعكوسة (المقلوبة):

(...

 $\vec{K}$ 

 $K = \frac{2\pi}{\lambda}$ 

.(

2-9-1 مفهوم الشبكة المعكوسة:

 $(\sin \theta_{hkl} = n\lambda/2d_{hkl})$ :  $(\sin(\theta_{hkl}))$   $(d_{hkl})$ 

 $(\sin( heta_{hkl}))$ 

2-9-2 خصائص الشبكة المعكوسة:

 $\left(d_{hkl}
ight)$   $\left(\begin{array}{c} 2\pi \end{array}\right)$ 

.

 $(\vec{K})$ 

 $\vec{G} = \vec{A}_1 g_1 + \vec{A}_2 g_2 + \vec{A}_3 g_3$ (8-2) $\vec{A}_1, \vec{A}_2, \vec{A}_3$  $g_1, g_2, g_3$  $\vec{A}_1, \vec{A}_2, \vec{A}_3$  $\vec{a}_1, \vec{a}_2, \vec{a}_3$  (  $\vec{A}_1.\vec{a}_1 = 2\pi \qquad \qquad \vec{A}_1.\vec{a}_2 = 0$  $\vec{A}_1.\vec{a}_3=0$  $\vec{A}_2 \vec{a}_2 = 2\pi$   $\vec{A}_2 \cdot \vec{a}_1 = 0$   $\vec{A}_2 \cdot \vec{a}_3 = 0$   $\vec{A}_3 \cdot \vec{a}_3 = 2\pi$   $\vec{A}_3 \cdot \vec{a}_1 = 0$   $\vec{A}_3 \cdot \vec{a}_2 = 0$ (9-2) $\vec{A}_3$  $(\vec{a}_2 \times \vec{a}_3 / \vec{a}_2 \times \vec{a}_3)$ : (9-2)  $(\vec{a}_3 \times \vec{a}_1 / \vec{a}_3 \times \vec{a}_1)$ :  $(\vec{a}_1 \times \vec{a}_2 / \vec{a}_1 \times \vec{a}_2)$  $\vec{A}_1 \cdot \vec{a}_1 = 2\pi \frac{\vec{a}_2 \times \vec{a}_3}{\vec{a}_2 \times \vec{a}_2} \Rightarrow \vec{A}_1 = 2\pi \frac{\vec{a}_2 \times \vec{a}_3}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_2)}$  $\vec{A}_3 \cdot \vec{a}_3 = 2\pi \frac{\vec{a}_1 \times \vec{a}_2}{\vec{a}_1 \times \vec{a}_2} \Rightarrow \vec{A}_3 = 2\pi \frac{\vec{a}_1 \times \vec{a}_2}{\vec{a}_2 \cdot (\vec{a}_1 \times \vec{a}_2)}$ (10-2) $\vec{A}_2 \cdot \vec{a}_2 = 2\pi \frac{\vec{a}_3 \times \vec{a}_1}{\vec{a}_2 \times \vec{a}_1} \Rightarrow \vec{A}_2 = 2\pi \frac{\vec{a}_3 \times \vec{a}_1}{\vec{a}_2 \cdot (\vec{a}_2 \times \vec{a}_1)}$  $(\vec{A}_1, \vec{A}_2, \vec{A}_3)$  $\vec{a}_1(\vec{a}_2 \times \vec{a}_3)$   $\vec{a}_2(\vec{a}_3 \times \vec{a}_1)$   $\vec{a}_3(\vec{a}_1 \times \vec{a}_2)$ (10-2)(11-2) $V_e = \vec{a}_1(\vec{a}_2 \times \vec{a}_3) = \vec{a}_2(\vec{a}_3 \times \vec{a}_1) = \vec{a}_3(\vec{a}_1 \times \vec{a}_2)$  $(\vec{A}_1, \vec{A}_2, \vec{A}_3)$ 

 $(\vec{K})$  $V_{e}^{*}$  $V_{e}$  $V_e^* V_e = (\vec{A}.(\vec{A}_2 \times \vec{A}_3))(\vec{a}_1.(\vec{a}_2 \times \vec{a}_3)) = \begin{vmatrix} \vec{A}_1.\vec{a}_1 & \vec{A}_1.\vec{a}_2 & \vec{A}_1.\vec{a}_3 \\ \vec{A}_2.\vec{a}_1 & \vec{A}_2.\vec{a}_2 & \vec{A}_2.\vec{a}_3 \\ \vec{A}_3.\vec{a}_1 & \vec{A}_3.\vec{a}_2 & \vec{A}_3.\vec{a}_3 \end{vmatrix} = (2\pi)^3$  $\vec{R}$  $\vec{G}.\vec{R} = (\vec{A}_1g_1 + \vec{A}_2g_2 + \vec{A}_3g_3).(n_1\vec{a}_1 + n_2\vec{a}_2 + n_3\vec{a}_3)$  $=2\pi(g_1n_1+g_2n_2+g_3n_3)$ (13-2) $=2\pi m$  $\vec{G}_{hkl} = h\vec{A}_1 + k\vec{A}_2 + l\vec{A}_3$ : (hkl):((15.2)  $\overrightarrow{p_1}\overrightarrow{p_2} = \left(\frac{\overrightarrow{a_2}}{k}\right) - \left(\frac{\overrightarrow{a_1}}{k}\right) \quad \mathcal{I} \quad \overrightarrow{p_1}\overrightarrow{p_3} = \left(\frac{\overrightarrow{a_3}}{k}\right) - \left(\frac{\overrightarrow{a_1}}{k}\right)$  $\vec{G}_{hkl} \cdot \overrightarrow{p_1 p_2} = \left(h\vec{A}_1 + k\vec{A}_2 + l\vec{A}_3\right) \cdot \left(\left(\frac{\vec{a}_2}{k}\right) - \left(\frac{\vec{a}_1}{h}\right)\right) = -2\pi + 2\pi = 0 \Rightarrow \vec{G}_{hkl} \perp \overrightarrow{p_1 p_2}$  $\vec{G}_{hkl}.\overrightarrow{p_1p_3} = \left(h\vec{A}_1 + k\vec{A}_2 + l\vec{A}_3\right).\left(\left(\frac{\vec{a}_3}{l}\right) - \left(\frac{\vec{a}_1}{h}\right)\right) = -2\pi + 2\pi = 0 \Rightarrow \vec{G}_{hkl} \perp \overrightarrow{p_1p_3}$  $\lfloor (hkl) \overline{\perp \vec{G}_{hkl}}$ :  $\vec{G}_{hkl} \perp \overline{p_1 p_2}$   $\vec{G}_{hkl} \perp \overline{p_1 p_3}$ : (14-2)

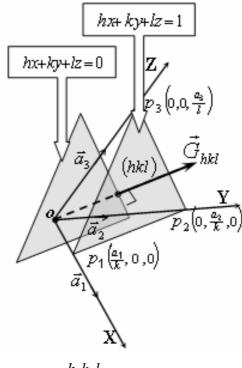
$$||\overrightarrow{OP}|| = d_{hkl} : \qquad (15.2)$$

$$\vec{G}_{hkl}.\overrightarrow{Op_1} = \left(h\vec{A}_1 + k\vec{A}_2 + l\vec{A}_3\right)\left(\frac{\vec{a}_1}{h}\right) = 2\pi :$$

$$\vec{G}_{hkl}.\overrightarrow{Op_1} = \|\vec{G}_{hkl}\| \|\overrightarrow{Op_1}\| \cos(\vec{G}_{hkl}, \overrightarrow{Op_1}) = \|\vec{G}_{hkl}\| \|\overrightarrow{OP}\| = \|\vec{G}_{hkl}\| d_{hkl} :$$

 $d_{hkl}$ 

(15-2) 
$$\|\vec{G}_{hkl}\| d_{hkl} = 2\pi \Rightarrow \|\vec{G}_{hkl}\| = \frac{2\pi}{d_{hkl}} :$$



.(hkl) h,k,l :(15.2)

#### 2-9-3 حساب القيم المعكوسة(المقلوبة):

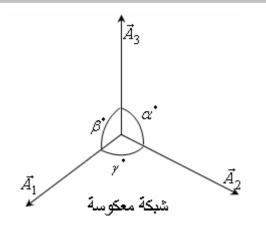
$$\alpha = (\vec{a}_2, \vec{a}_3) : \qquad \vec{a}_1, \vec{a}_2, \vec{a}_3 : \\ \alpha^* = (\vec{A}_2, \vec{A}_3) : \qquad \vec{A}_1, \vec{A}_2, \vec{A}_3 \qquad \qquad .\gamma = (\vec{a}_1, \vec{a}_2) \quad \beta = (\vec{a}_3, \vec{a}_1) \\ .\gamma^* = (\vec{A}_1, \vec{A}_2) \quad \beta^* = (\vec{A}_3, \vec{A}_1)$$

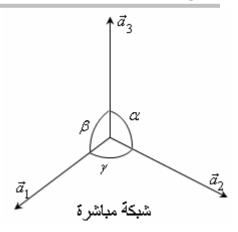
:((15.2)

#### • حساب الزوايا المعكوسة:

$$(16-2) \qquad V_e = \vec{a}_1(\vec{a}_2 \times \vec{a}_3) = \vec{a}_2(\vec{a}_3 \times \vec{a}_1) = \vec{a}_3(\vec{a}_1 \times \vec{a}_2) :$$

$$\vec{A}_1 = 2\pi \frac{\vec{a}_2 \times \vec{a}_3}{V_e} , \quad \vec{A}_3 = 2\pi \frac{\vec{a}_1 \times \vec{a}_2}{V_e} , \quad \vec{A}_2 = 2\pi \frac{\vec{a}_3 \times \vec{a}_1}{V_e}$$





:(15.2)

$$\vdots \qquad \left(\vec{A}_1 \cdot \vec{A}_2\right)$$

(17-2) 
$$\vec{A}_{1}. \vec{A}_{2} = 2\pi \frac{\vec{a}_{2} \times \vec{a}_{3}}{V_{e}}.2\pi \frac{\vec{a}_{3} \times \vec{a}_{1}}{V_{e}} = \frac{4\pi^{2}}{V_{e}^{2}} (\vec{a}_{2} \times \vec{a}_{3}). (\vec{a}_{3} \times \vec{a}_{1})$$

:

(18-2) 
$$(\vec{a}_2 \times \vec{a}_3)$$
.  $(\vec{a}_3 \times \vec{a}_1) = (\vec{a}_2 \cdot \vec{a}_3) (\vec{a}_3 \cdot \vec{a}_1) - (\vec{a}_2 \times \vec{a}_1) \cdot a_3^2 = a_2 a_3^2 a_1 (\cos(\alpha)\cos(\beta) - \cos(\gamma))$ 

(19-2) 
$$\vec{A}_1 \cdot \vec{A}_2 = \frac{4\pi^2}{V_e^2} a_1 a_2 a_3^2 (\cos(\alpha)\cos(\beta) - \cos(\gamma))$$

•

$$\vec{A}_{1}. \ \vec{A}_{2} = \left\| \vec{A}_{1} \right\| \left\| \vec{A}_{2} \right\| \cos \left( \gamma^{*} \right) = \frac{4\pi^{2}}{V_{e}^{2}} \left\| \vec{a}_{2} \times \vec{a}_{3} \right\| \left\| \vec{a}_{3} \times \vec{a}_{1} \right\| \cos \left( \gamma^{*} \right)$$

(20-2) 
$$\vec{A}_1 \cdot \vec{A}_2 = \frac{4\pi^2}{V_a^2} a_1 a_2 a_3^2 \sin(\alpha) \sin(\beta) \cos(\gamma^*)$$

(21-2) 
$$\cos(\gamma^*) = \frac{\cos(\alpha)\cos(\beta) - \cos(\gamma)}{\sin(\alpha)\sin(\beta)}$$

$$\cos(\beta^*)\cos(\alpha^*)$$

(22-2) 
$$\cos(\alpha^*) = \frac{\cos(\beta)\cos(\gamma) - \cos(\alpha)}{\sin(\beta)\sin(\gamma)}$$

(23-2) 
$$\cos(\beta^*) = \frac{\cos(\gamma)\cos(\alpha) - \cos(\beta)}{\sin(\lambda)\sin(\alpha)}$$

#### • حساب الثوابت المعكوسة:

:

$$V_{e}^{2} = \left[\vec{a}_{1}(\vec{a}_{2} \times \vec{a}_{3})\right]^{2} = \begin{vmatrix} \vec{a}_{1}.\vec{a}_{1} & \vec{a}_{1}.\vec{a}_{2} & \vec{a}_{1}.\vec{a}_{3} \\ \vec{a}_{2}.\vec{a}_{1} & \vec{a}_{2}.\vec{a}_{2} & \vec{a}_{2}.\vec{a}_{3} \\ \vec{a}_{3}.\vec{a}_{1} & \vec{a}_{3}.\vec{a}_{2} & \vec{a}_{3}.\vec{a}_{3} \end{vmatrix} \Rightarrow$$

$$(24-2) \qquad V_{e}^{2} = (a_{1}a_{2}a_{3})^{2} \left(1 + 2\cos(\alpha)\cos(\beta)\cos(\gamma) - \cos^{2}(\alpha) - \cos^{2}(\beta) - \cos^{2}(\gamma)\right)$$

$$\vdots \|\vec{A}_{1}\|^{2}$$

$$\|\vec{A}_1\|^2 = \frac{4\pi^2}{V_e^2} \|\vec{a}_2 \times \vec{a}_3\|^2$$

$$\|\vec{A}_1\|^2 = \frac{4\pi^2}{(a_1 a_2 a_3)^2 (1 + 2\cos\alpha\cos\beta\cos\gamma - (\cos\alpha)^2 - (\cos\beta)^2 - (\cos\gamma)^2)} (a_2 a_3)^2 (\sin(\alpha))^2$$

(25-2) 
$$\|\vec{A}_1\|^2 = \frac{(\sin(\alpha))^2}{(1 + 2\cos\alpha\cos\beta\cos\gamma - \cos^2(\alpha) - \cos^2(\beta) - \cos^2(\gamma))} \left(\frac{2\pi}{a_1}\right)^2$$
$$: \|\vec{A}_3\|^2 \|\vec{A}_2\|^2$$

(26-2) 
$$\|\vec{A}_2\|^2 = \frac{(\sin(\beta))^2}{(1 + 2\cos\alpha\cos\beta\cos\gamma - \cos^2(\alpha) - \cos^2(\beta) - \cos^2(\gamma))} (\frac{2\pi}{a_2})^2$$

(27-2) 
$$\|\vec{A}_1\|^2 = \frac{(\sin(\gamma))^2}{(1 + 2\cos\alpha\cos\beta\cos\gamma - \cos^2(\alpha) - \cos^2(\beta) - \cos^2(\gamma))} \left(\frac{2\pi}{a_3}\right)^2$$

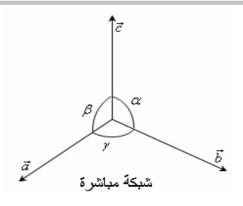
#### : $(d_{hkl})$ العلاقة العامة للمسافة الفاصلة بين المستويات البلورية المتوازية المسافة الفاصلة بين المستويات البلورية المسافة الفاصلة بين المستويات البلورية المتوازية المسافة الفاصلة بين المستويات المستويا

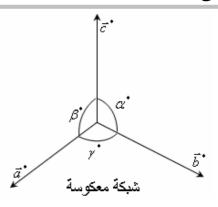
$$d_{hkl}$$

$$(X,Y,Z)$$

$$\gamma = (\vec{a},\vec{b}) \quad \beta = (\vec{c},\vec{a}) \quad \alpha = (\vec{b},\vec{c}) : \quad \vec{c},\vec{b},\vec{a}$$

$$\beta^* = (\vec{c}^*,\vec{a}^*) \quad \alpha^* = (\vec{b}^*,\vec{c}^*) : \quad \vec{c}^*,\vec{b}^*,\vec{a}^* : \quad ((16.2) \quad )\gamma^* = (\vec{a}^*,\vec{b}^*)$$





:(16.2)

•

- - 
$$(d_{hkl})$$

:

 $\alpha \neq \beta \neq \gamma \quad a \neq b \neq c$ 

$$\|\vec{G}_{hkl}\| = \frac{2\pi}{d_{hkl}} \Rightarrow \frac{1}{(d_{hkl})^2} = \frac{\|\vec{G}_{hkl}\|^2}{(2\pi)^2} \Rightarrow \frac{1}{(d_{hkl})^2} = \frac{\vec{G}_{hkl} \cdot \vec{G}_{hkl}}{(2\pi)^2}$$

$$\vec{G}_{hkl} \cdot \vec{G}_{hkl} = (h\vec{a}_1^* + k\vec{a}_2^* + l\vec{a}_3^*)(h\vec{a}_1^* + k\vec{a}_2^* + l\vec{a}_3^*)$$

$$\vec{G}_{hkl} \cdot \vec{G} = h^2 \|\vec{a}_1^*\|^2 + k^2 \|\vec{a}_2^*\|^2 + l^2 \|\vec{a}_3^*\|^2 + 2 \|\vec{a}_1^*\| \|\vec{a}_2^*\| \cos \gamma^*$$

$$+ 2 \|\vec{a}_2^*\| \|\vec{a}_3^*\| \cos \alpha^* + 2 \|\vec{a}_3^*\| \|\vec{a}_1^*\| \cos \beta^*$$

$$(27-2) \quad (26-2) \quad (25-2) \quad (23-2) \quad (22-2) \quad (21-2)$$

(28

.

$$(29-2) \frac{1}{(d_{hkl})^{2}} = \frac{a^{2}b^{2}c^{2}}{v^{2}} \left( \frac{h^{2}\sin^{2}(\alpha)}{a^{2}} + \frac{k^{2}\sin^{2}(\beta)}{b^{2}} + \frac{l^{2}\sin^{2}(\gamma)}{c^{2}} + \frac{2hk}{ab}(\cos(\alpha)\cos(\beta) - \cos(\gamma)) + \frac{2kl}{bc}(\cos(\beta)\cos(\gamma) - \cos(\beta)) + \frac{2hl}{ac}(\cos(\gamma)\cos(\alpha) - \cos(\beta)) \right)$$

(30-2)  $v^{2} = (abc)^{2} (1 + 2\cos(\alpha)\cos(\beta)\cos(\gamma) - \cos^{2}(\alpha) - \cos^{2}(\beta) - \cos^{2}(\gamma))$ 

$$\alpha = \gamma = \frac{\pi}{2} \neq \beta \quad \text{s} \quad a \neq b \neq c \quad \therefore$$
 .1

69

(31-2) 
$$\frac{1}{(d_{hkl})^2} = \frac{1}{\sin^2(\beta)} \left( \frac{h^2}{a^2} + \frac{k^2 \sin^2(\beta)}{b^2} + \frac{l^2}{c^2} - \frac{2hl}{ac} (\cos(\beta)) \right)$$

$$\alpha = \gamma = \beta = \frac{\pi}{2} \quad \text{3} \quad a \neq b \neq c \quad .2$$

(32-2) 
$$\frac{1}{(d_{hkl})^2} = \left(\frac{h^2}{a^2} + \frac{k^2}{b^2} + \frac{l^2}{c^2}\right)$$

$$\alpha = \gamma = \beta = \frac{\pi}{2} \quad \mathcal{I} \quad a = b \neq c \quad \therefore$$
 3

(33-2) 
$$\frac{1}{(d_{hkl})^2} = \left(\frac{h^2 + k^2}{a^2} + \frac{l^2}{c^2}\right)$$

$$\alpha = \gamma = \beta = \frac{\pi}{2} \quad \beta \quad a = b = c \quad .4$$

(34-2) 
$$\frac{1}{(d_{hkl})^2} = \left(\frac{h^2 + k^2 + l^2}{a^2}\right)$$

$$\alpha = \gamma = \beta \neq \frac{\pi}{2} < 120^{\circ} \quad \beta \quad a = b = c \quad .5$$

(35-2) 
$$\frac{1}{(d_{hkl})^2} = \frac{(h^2 + k^2 + l^2)\sin^2(\alpha) + 2(hk + kl + hl)(\cos^2(\alpha) - \cos(\alpha))}{a^2(1 + 2\cos^3(\alpha) - 3\cos^2(\alpha))}$$

$$\alpha = \beta = \frac{\pi}{2}, \gamma = 120^{\circ} \quad \text{3} \quad a = b \neq c \quad .6$$

(36-2) 
$$\frac{1}{(d_{hkl})^2} = \frac{4}{3} \left( \frac{(h^2 + hk + k^2)}{a^2} \right) + \frac{l^2}{c^2}$$

#### 2-9-5 إنشاء شبكة مستوية معكوسة لشبكة مستوية مباشرة:

$$\gamma$$
  $\vec{a}_1, \vec{a}_2$  .1

$$d_{010} \quad d_{100} \qquad (010) \quad (100)$$

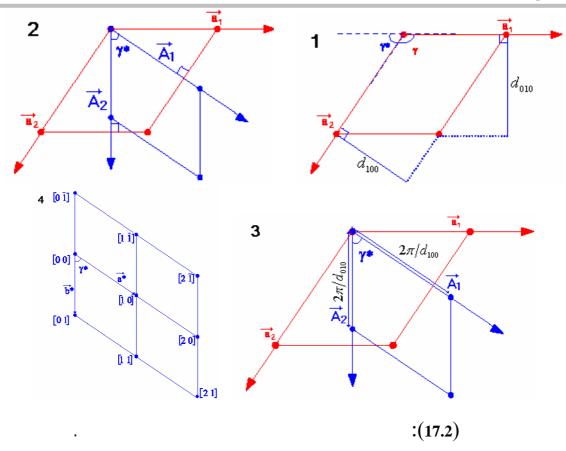
$$\vec{a}_1, \vec{A}_2$$
  $\vec{a}_2$   $\vec{a}_1$  .2

1/

$$||\vec{A}_2|| = 2\pi/d_{010}$$
  $d_{hkl}$   $\vec{A}_1, \vec{A}_2$  .3

$$\|\vec{A}_1\| = 2\pi/d_{100}$$

$$.\vec{G}_{hk} = h\vec{A}_1 + k\vec{A}_2$$
 .4



# 2-9-6 شروط فون لاوي للانعراج:

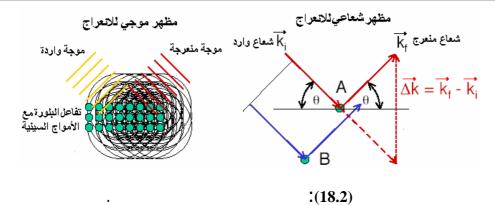
$$(\lambda_f) \qquad (\lambda_i)$$

$$\cdot \qquad \left\|\vec{K}_f\right\| = 2\pi/\lambda_f\right) \qquad \left\|\vec{K}_i\right\| = 2\pi/\lambda_i\right)$$

$$\vdots \qquad \dot{\vec{K}} \qquad \vec{K}$$

$$\Delta \vec{K} = \vec{K}_f - \vec{K}_i$$

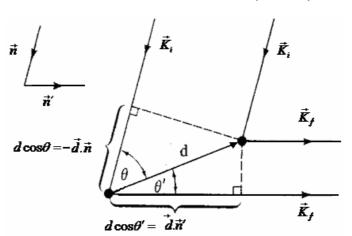
(19.2)



$$\vec{n}' \quad \vec{K}_f \qquad \qquad \vec{n} \quad \vec{K}_i \\ \vec{d} = \vec{a}_i (i = 1, 2, 3):$$

 $\vec{n}' \quad \vec{n} : \quad .$ 

(38-2)  $d\cos\theta + d\cos\theta' = \vec{d}.(\vec{n}' - \vec{n})$ 



•

(39-2) 
$$\vec{d} \cdot (\vec{n}' - \vec{n}) = m\lambda$$

$$\vdots \qquad \left(\frac{2\pi}{\lambda}\right) \qquad (39-2)$$

$$\vec{d} \cdot \left[ \left( \frac{2\pi}{\lambda} \right) \cdot \vec{n}' - \left( \frac{2\pi}{\lambda} \right) \cdot \vec{n} \right] = 2\pi m$$

$$\vec{d} \cdot (\vec{K}_f - \vec{K}_i) = 2\pi m$$

$$(40-2) \vec{d} \cdot (\Delta \vec{k}) = 2\pi m$$

 $\vec{d} = \vec{a}_i (i = 1, 2, 3) :$ 

(41-2) 
$$\vec{a}_1 \cdot (\Delta \vec{k}) = 2\pi m_1$$

(42-2) 
$$\vec{a}_2 \cdot (\Delta \vec{k}) = 2\pi m_2$$

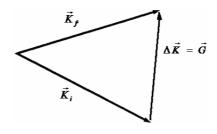
$$\vec{a}_3.(\Delta \vec{k}) = 2\pi m_3$$

, 
$$\left(\overrightarrow{\Delta K}\right)$$
 ,  $\left(43-2\right)$   $\left(42-2\right)$   $\left(41-2\right)$   $\left(\overrightarrow{\Delta K}\right)$   $\left(13-2\right)$ 

: ((20.2) )

$$\Delta \vec{k} = \vec{G}$$

$$\vec{K}_f = \vec{K}_i + \vec{G}$$



(20.2)

: (45-2)

(46-2) 
$$K_f^2 = K_i^2 + G^2 + 2\vec{K}_i \cdot \vec{G}$$

73

$$\left\| \vec{K}_f \, \right\| = \left\| \vec{K}_i \right\| = \left\| \vec{K} \right\| = k$$

(47-2) 
$$G^2 + 2\vec{K}.\vec{G} = 0$$

(47-2)

#### 7-9-2 إنشاء إيوالد (Ewald):

: (

مسئوي الانجراج في الشبكة المباشرة مسئوية معكوسة مسئوية مسئوية في الشبكة المباشرة منحرج معكوسة مسئوية في الشبكة المباشرة منحرجة منحرجة أشعة خرمة أشعة خرمة أشعة خرمة أشعة منحرجة منحرجة منحرجة المباشرة منحرجة منحرجة منحرجة المباشرة منحرجة المباشرة منحرجة المباشرة منحرجة المباشرة منحرجة المباشرة منحرجة المباشرة المباشر

(21.2): إنشاء إيوالد.

 $\overrightarrow{AO} = \overrightarrow{K}_{i} \qquad , A \qquad \qquad \overrightarrow{||AO||} = ||\overrightarrow{K}_{i}|| = k = 2\pi/\lambda$   $|\overrightarrow{AO}| \qquad A \qquad \qquad \lambda$   $A \qquad \overrightarrow{AB} \qquad \qquad ,((21.2) \qquad )$   $(\overrightarrow{AB} = \overrightarrow{K}_{f}) \qquad B$   $\overrightarrow{OB} \qquad .(\overrightarrow{K}_{f} \qquad \qquad \overrightarrow{K}_{i} \qquad ($ 

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(PQ) (A) 
$$\|\vec{G}\|$$

(A)

 $\theta$ 

$$\|\vec{G}\| = \|\overrightarrow{\Delta k}\| = \frac{2\pi}{d} \Rightarrow d = \frac{2\pi}{\|\vec{G}\|}$$

(21.2)

$$\sin \theta = \frac{\frac{1}{2} \|\vec{G}\|}{\|\vec{K}\|} \Rightarrow \|\vec{G}\| = 2 \|\vec{K}\| \sin \theta \Rightarrow \frac{2\pi}{d} = 2 \cdot \frac{2\pi}{\lambda} \sin \theta \Rightarrow$$

(49-2) $\lambda = 2d \sin \theta$ 

> : (n) (n=1)(49-2)

 $n\lambda = 2d\sin\theta$ (50-2)

(21.2)

(51-2) 
$$\Delta \vec{k} = \vec{G} = \vec{K}_f - \vec{K}_i \Rightarrow \vec{K}_f = \vec{K}_i + \vec{G}$$

(51-2)

(52-2) 
$$K_f^2 = K_i^2 + G^2 + 2\vec{K}_i \cdot \vec{G}$$

: (52-2)  $\left\| \vec{K}_{f} \right\| = \left\| \vec{K}_{i} \right\| = \left\| \vec{K} \right\| = k :$ (21.2)

(53-2) 
$$G^2 + 2\vec{K}.\vec{G} = 0$$

(53-2)

#### 8-9-2 مناطق بريلوان (Brilloun):

(Wigner-Seitz)

$$\vec{G}$$
 (47-2)

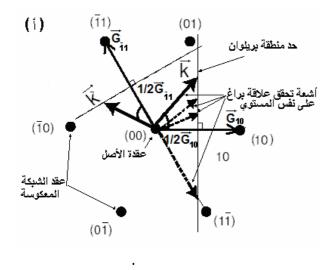
 $: -\vec{G} \quad \vec{G}$  $-\vec{G}$ (47-2)

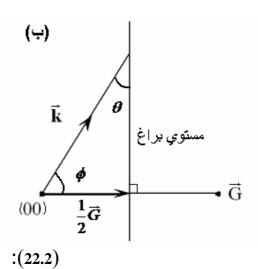
$$2\vec{k}.\vec{G} = G^2 \Rightarrow \vec{K}.\vec{G} = \frac{1}{2}G^2 \Rightarrow ||\vec{K}||.||\vec{G}||\cos\phi = \frac{1}{2}G^2 \Rightarrow$$

$$\left\| \vec{K} \right\| \cos \phi = \frac{1}{2} \left\| \vec{G} \right\|$$

$$egin{aligned} & (()(22.2)) & ()(22.2) & \vec{G} \ & (\cos\phi = \sin heta) & ()(22.2) & () \end{aligned}$$

(55-2)  $K\cos\phi = K\sin\theta = \frac{1}{2}G \Rightarrow \frac{2\pi}{\lambda}\sin\theta = \frac{1}{2}\cdot\frac{2\pi}{d} \Rightarrow \lambda = 2d\sin\theta$ 



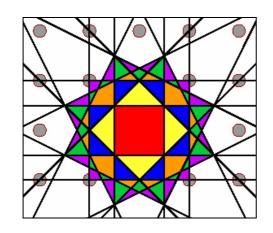


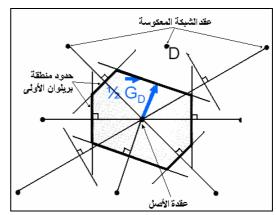
( )

:

( )  $ec{G}$ 

.





:(23.2)

بعض خصائص مناطق بريلوان:

.1

. . .2

: .3

#### 2-9-9 معكوس شبكات الفئة المكعبة:

:

1. معكوس الشبكة المكعبة البسيطة (CS):

$$\vec{a}_1 = a \, \vec{i} \quad , \quad \vec{a}_2 = a \, \vec{j} \quad , \quad \vec{a}_3 = a \, \vec{k} \quad :$$

$$\vdots$$

$$\vec{A}_1 = 2\pi \, \frac{\vec{a}_2 \times \vec{a}_3}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3)} = 2\pi \, \frac{a^2}{a^3} (\vec{j} \times \vec{k}) = \frac{2\pi}{a} \, \vec{i}$$

$$\vec{A}_2 = 2\pi \, \frac{\vec{a}_3 \times \vec{a}_1}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3)} = 2\pi \, \frac{a^2}{a^3} (\vec{k} \times \vec{i}) = \frac{2\pi}{a} \, \vec{j}$$

$$\vec{A}_3 = 2\pi \, \frac{\vec{a}_1 \times \vec{a}_2}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3)} = 2\pi \, \frac{a^2}{a^3} (\vec{i} \times \vec{j}) = \frac{2\pi}{a} \, \vec{k}$$

 $\vec{A}_1, \vec{A}_2, \vec{A}_3$ 

 $.2\pi/a$ 

 $2\pi/a$ 

$$V_{SB}^{CS} = \vec{A}_1 \cdot (\vec{A}_2 \times \vec{A}_3) = \left(\frac{2\pi}{a}\right)^3 : \qquad . \pm \vec{A}_1 = \pm \frac{2\pi}{a} \vec{i}, \pm \vec{A}_2 = \pm \frac{2\pi}{a} \vec{j}, \pm \vec{A}_3 = \pm \frac{2\pi}{a} \vec{k} :$$

2. معكوس الشبكة المكعبة الممركزة (CC):

.1

$$\vec{a}_3 = \frac{a}{2} (\vec{i} + \vec{j} - \vec{k})$$
  $\vec{a}_2 = \frac{a}{2} (\vec{i} - \vec{j} + \vec{k})$   $\vec{a}_1 = \frac{a}{2} (-\vec{i} + \vec{j} + \vec{k})$ 

:

(56-2) 
$$\vec{A}_{1} = 2\pi \frac{\vec{a}_{2} \times \vec{a}_{3}}{\vec{a}_{1} \cdot (\vec{a}_{2} \times \vec{a}_{3})} = 2\pi \frac{\left(a^{2} / 4\right)}{\left(a^{3} / 2\right)} \left(\left(\vec{i} - \vec{j} + \vec{k}\right) \times \left(\vec{i} + \vec{j} - \vec{k}\right)\right) = \frac{\pi}{a} \left(\vec{k} + \vec{j} + \vec{k} + \vec{i} + \vec{j} - \vec{i}\right)$$
$$= \frac{2\pi}{a} \left(\vec{k} + \vec{j}\right)$$

:

(57-2) 
$$\vec{A}_2 = 2\pi \frac{\vec{a}_3 \times \vec{a}_1}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3)} = \frac{2\pi}{a} (\vec{i} + \vec{k})$$

(58-2) 
$$\vec{A}_3 = 2\pi \frac{\vec{a}_1 \times \vec{a}_2}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3)} = \frac{2\pi}{a} (\vec{j} + \vec{i})$$

CFC 
$$\vec{A}_1, \vec{A}_2, \vec{A}_3$$
 
$$\big)4\pi/a$$

.

\_

((24.2) ) 
$$\frac{2\pi}{a} \left( \pm \vec{j} \pm \vec{i} \right) , \frac{2\pi}{a} \left( \pm \vec{i} \pm \vec{k} \right) , \frac{2\pi}{a} \left( \pm \vec{k} \pm \vec{j} \right) :$$

$$V_{SB}^{CC} = \vec{A}_1 \cdot (\vec{A}_2 \times \vec{A}_3) = 2 \left(\frac{2\pi}{a}\right)^3$$

#### 3. معكوس الشبكة المكعبة الممركزة الأوجه (CFC):

:

$$\vec{a}_3 = \frac{a}{2} \left( \vec{i} + \vec{j} \right) \qquad \vec{a}_2 = \frac{a}{2} \left( \vec{i} + \vec{k} \right) \qquad \vec{a}_1 = \frac{a}{2} \left( \vec{j} + \vec{k} \right)$$

(59-2)  $\vec{A}_1 = 2\pi \frac{\vec{a}_2 \times \vec{a}_3}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3)} = 2\pi \frac{\left(a^2/4\right)}{\left(a^3/4\right)} \left(\left(\vec{i} + \vec{k}\right) \times \left(\vec{i} + \vec{j}\right)\right) = \frac{2\pi}{a} \left(\vec{k} + \vec{j} - \vec{i}\right) = \frac{2\pi}{a} \left(-\vec{i} + \vec{j} + \vec{k}\right)$ 

:

(60-2) 
$$\vec{A}_2 = 2\pi \frac{\vec{a}_3 \times \vec{a}_1}{\vec{a}_1 \cdot (\vec{a}_2 \times \vec{a}_3)} = \frac{2\pi}{a} (\vec{i} - \vec{j} + \vec{k})$$

(61-2) 
$$\vec{A}_{3} = 2\pi \frac{\vec{a}_{1} \times \vec{a}_{2}}{\vec{a}_{1} \cdot (\vec{a}_{2} \times \vec{a}_{3})} = \frac{2\pi}{a} (\vec{i} + \vec{j} - \vec{k})$$

CC

 $\vec{A}_1, \vec{A}_2, \vec{A}_3$ 

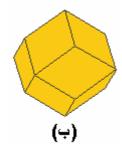
 $.4\pi/a$ 

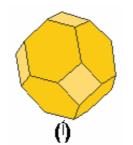
CC

((24.2) )( )

$$\frac{2\pi}{a} \left( \pm \vec{i} \pm \vec{k} \pm \vec{j} \right)$$
:

$$.V_{SB}^{CFC} = \vec{A}_1 . (\vec{A}_2 \times \vec{A}_3) = 4 \left(\frac{2\pi}{a}\right)^3 : \pm \frac{4\pi}{a} \vec{K} , \pm \frac{4\pi}{a} \vec{j} , \pm \frac{4\pi}{a} \vec{i} :$$





. (ب) *CC* 

(i) CFC

:(24.2)

2-10 عامل البنية:

( ) .

•

$$\vec{a}, \vec{b}, \vec{c}$$
 
$$(\vec{r}_j = x_j \vec{a} + y_j \vec{b} + z_j \vec{c}) :$$

$$\vec{r}_{j}$$
 . 
$$(\vec{R}_{m,n,p}) \qquad \qquad : \qquad . \vec{R}_{0,0,0} \qquad \qquad (\vec{R}_{m,n,p} = m \, \vec{a} + n \, \vec{b} + p \, \vec{c})$$

.((25.2) )
$$(\vec{r}_j + \vec{R}_{m,n,p})$$
:  $(\vec{R}_{m,n,p})$ 

.

: 
$$(j) C_{j}$$
 
$$C_{j} \left( \vec{R} - \left( \vec{r}_{j} + \vec{R}_{m,n,p} \right) \right)$$

 $(62-2) C_j \left(R - \left(\vec{r}_j + R_{m,j}\right)\right)$ 

 $ec{R}$  : .

,  $C_j$ 

:

(63-2) 
$$N(\vec{r}') = \sum_{j=1}^{S} C_{j} \left( \vec{R} - \left( \vec{r}_{j} + \vec{R}_{m,n,p} \right) \right)$$

$$.S \qquad \qquad (j) \qquad \vec{r}' = \vec{R} - \left( \vec{r}_{j} + \vec{R}_{m,n,p} \right) :$$

$$\vec{\Omega} \qquad ($$

:

(64-2) 
$$\Omega = \sum_{mnp}^{M^3} \int_{\exists L \subseteq S} N(\vec{r}') e^{i\vec{R} \cdot \overrightarrow{\Delta k}} dv$$

$$M^3 \qquad (mnp)$$

(64-2)

$$\Omega = \sum_{mnp}^{M^3} \sum_{j}^{S} \int_{\vec{k} = \vec{k}} C_j(\vec{r}') dv e^{i(\vec{r}' + \vec{R}_{m,n,p} + \vec{r}_j) \cdot \overrightarrow{\Delta k}}$$

(65-2) 
$$\Omega = \sum_{mnp}^{M^3} \sum_{j}^{S} f_j e^{i(\vec{R}_{m,n,p} + \vec{r}_j) \cdot \Delta \vec{k}}$$

•

 $f_{j}$ 

$$f_{j} = \int_{i \neq k} C_{j}(\vec{r}') \, dv \, e^{i\vec{r}' \cdot \overrightarrow{\Delta k}}$$

. (j)

 $\vec{\Delta k} = \vec{G}$ 

$$\Omega = M^{3} \sum_{j}^{S} f_{j} e^{i\vec{r}_{j}.\vec{G}} e^{i\vec{R}_{m,n,p}.\vec{G}} = M^{3} \sum_{j}^{S} f_{j} e^{i\vec{r}_{j}.\vec{G}} \cdot \left(e^{i\vec{R}_{m,n,p}.\vec{G}} = 1\right)$$

 $\Omega = M^3 F$ 

(67-2) 
$$F = \sum_{j}^{S} f_{j} e^{i\vec{r}_{j}.\vec{G}}$$

: F

$$\vec{r}_{j}.\vec{G} = (x_{j}\vec{a} + y_{j}\vec{b} + z_{j}\vec{c})(h\vec{a}^{*} + k\vec{b}^{*} + l\vec{c}^{*})$$

$$= 2\pi(x_{j}h + y_{j}k + z_{j}l)$$

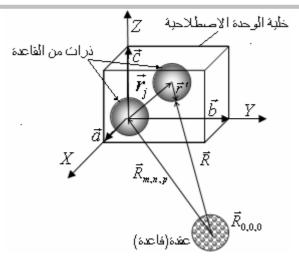
:

(68-2) 
$$F_{hkl} = \sum_{i}^{S} f_{i} e^{i2\pi(x_{j}h + y_{j}k + z_{j}l)}$$

 $F_{hkl}$ 

(hkl)

 $. \hspace{1cm} (hkl) \hspace{1cm} .$ 



. :(25.2)

## 2-11 حساب عامل البنية لبعض البني البلورية:

: (68-2)

• بنية المكعب البسيط (CS)

 $F_{hkl}$ 

(0,0,0):

$$F_{hkl}=f\ e^{i2\pi(0h+0k+0l)}=f$$
 
$$h,k,l\qquad F_{hkl}\qquad (F_{hkl}
eq 0)$$

• بنیة المکعب الممرکز (cc):

$$(0,0,0)$$
:  $((CS)$   $(CC)$   $(\frac{1}{2},\frac{1}{2},\frac{1}{2})$ :

$$F_{hkl} = f + f e^{i2\pi (h/2 + k/2 + l/2)} = f (1 + e^{i\pi(h+k+l)})$$

$$h_{j,k,l}$$

 $(F_{hkl} = 2f \neq 0)$  h+k+l=2n: h+k+l

$$(F_{hkl} = 0)$$
  $h+k+l=2n+1$ :  $h+k+l$ 

(hkl)

• بنية المكعب الممركز الأوجه (CFC): ))(CS)(CFC)(0,0,0):  $\left(0,\frac{1}{2},\frac{1}{2}\right)\left(\frac{1}{2},0,\frac{1}{2}\right)\left(\frac{1}{2},\frac{1}{2},0\right)$ :  $F_{hkl} = f \left( 1 + e^{i\pi(h+k)} + e^{i\pi(h+l)} + e^{i\pi(k+l)} \right)$  $F_{hkl}$ h, k, l $(F_{hkl}=0)$ h, k, l• بنیة کلورید السیزیوم (CsCl): )) $(Cs^+)$   $(((Cs^+)$   $(Cl^-)$  $(Cs^+)$  (CsCl) $\left(\frac{1}{2}, \frac{1}{2}, \frac{1}{2}\right)$ :  $(Cl^-)$ (0,0,0) $F_{hkl} = f_{Cs^{+}} + f_{Cl^{-}} e^{i\pi(h+k+l)}$  $F_{hkl}$ h, k, l $(F_{hkl} = f_{Cs^{+}} + f_{Cl^{-}} \neq 0)$  $(F_{hkl}=0)$ • بنية كلوريد الصوديوم (NaCl) )) $(Na^+)$  $(Cl^{-})$ (CS)(NaCl) $(Cl^-)$ (CFC) $(Na^+)$  $\cdot \left(0,0,\frac{1}{2}\right) \left(0,\frac{1}{2},0\right) \left(\frac{1}{2},0,0\right) \left(\frac{1}{2},\frac{1}{2},\frac{1}{2}\right) : \mathsf{CI}^{-} \left(\frac{1}{2},\frac{1}{2},0\right) \left(\frac{1}{2},0,\frac{1}{2}\right) \left(0,\frac{1}{2},\frac{1}{2}\right) (0,0,0) : \mathsf{Na}^{+}$ 

:

$$F_{hkl} = f_{Na^{+}} \left( 1 + e^{i\pi(h+k)} + e^{i\pi(h+l)} + e^{i\pi(k+l)} \right)$$

$$+ f_{Cl^{-}} \left( e^{i\pi(h+k+l)} + e^{i\pi h} + e^{i\pi k} + e^{i\pi l} \right)$$

$$: h, k, l \qquad F_{hkl}$$

$$. \qquad (F_{hkl} = 0) \qquad h, k, l$$

$$. \qquad (F_{hkl} = 4f_{Na^{+}} + 4f_{Cl^{-}}) \qquad h, k, l$$

$$. \qquad (F_{hkl} = 4f_{Na^{+}} - 4f_{Cl^{-}}) \qquad h, k, l$$

$$(+) \qquad (26.2)$$

NaCl	CsCl	CFC	CC	Cs	$N^2 = h^2 + k^2 + l^2$	(hkl)
-	+	-	-	+	1	(100)
-	+	-	+	+	2	(110)
+	+	+	-	+	3	(111)
+	+	+	+	+	4	(200)
-	+	-	-	+	5	(210)
-	+	-	+	+	6	(211)
+	+	+	+	+	8	(220)
-	+	-	-	+	9	(300) - (221)

. :(2.2)

الفصل الثالث

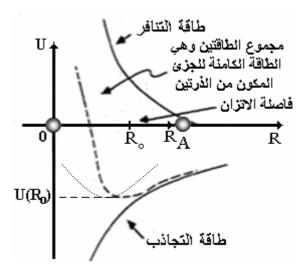
# الروابط البلورية والخصائص المرونية

```
3-1 مقدمة:
                   (
                                                  1. قوى التجادب:
                                                                       .1
                                                                       .2
                                            (Van DerWaals)
                                                                      .3
                                                     2. قوى التنافر:
                                                         : طاقة الترابط 2-3
                                                 .(
O
                                                              (1.3)
```

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( A r

F



الشكل (1.3):

$$\vec{F} = -\frac{dU}{dR}\frac{\vec{R}}{R}$$

 $\left( \qquad \right) \quad \frac{dU}{dR} > 0$  $\vec{F}$ (1.3)  $\vec{R}$  $\vec{R}$ (1.3) .( )  $\left( \begin{array}{c} \frac{dU}{dR} > 0 \end{array} \right)$  $R > R_0$  $(F)_{R_0} = 0$   $\frac{dU}{dR} = 0$   $R = R_0$   $\frac{dU}{dR} < 0$ 

 $R < R_0$ 

$$(2.3) U(R) = \frac{a}{R^m} - \frac{b}{R^n}$$

-b/R

 $a/R^m$ 

n, m, b, a:

$$\left(\frac{d^2U}{dR^2}\right)_{R_0} = \beta > 0 :$$

:  $\lambda \exp(-R/\rho)$ :

m>n

. *m* 

 $a/R^m$ 

 $\rho_{\iota}\lambda$ 

 $R_0$  (2.3)

:

$$(3.3) F(R_0) = \left(-\frac{du}{dr}\right)_{R=R_0} = 0$$

: 
$$R = R_0$$
 (3.3)

(2.3)

(4.3) 
$$-\left(\frac{bnR_0^{n-1}}{R_0^{2n}} - \frac{amR_0^{m-1}}{R_0^{2m}}\right) = 0$$

(4.3)

$$(5.3) R_0 = \left(\frac{am}{bn}\right)^{\frac{1}{m-n}}$$

:

 $(R = R_0)$  (2.3) (5.3)

(6.3) 
$$U(R_0) = \frac{bnR_0^{m-n}}{mR_0^m} - \frac{b}{R_0^n} = \frac{bn}{m}R_0^{-n} - \frac{b}{R_0^n} = -bR_0^{-n}\left(1 - \frac{n}{m}\right)$$

m > n أن

 $U\left(R_{0}\right) \tag{6.3}$ 

```
R > R_0
                                                                                              R = R_0
                                                                                 3-3 الرابطة الأيونية:
                      (CsCl)
                                                              (NaCl)
                               2N
                                        (2.3)
                                                                U_{ij} = \frac{a}{r_{ij}^{m}} \pm K \frac{q^2}{r_{ij}}
(7.3)
                        n=1 b=Kq^2
                                                                 \left(K = 1/4\pi\varepsilon_0 = 9 \times 10^9 \, Nm^2 / C^2\right)
                            (-)
                                                                     (+)
                                                    R: 	 r_{ij} = R p_{ij} 	 .
                        p_{ij}
                                                                R j i
                                 (7.3)
```

3

(8.3) 
$$U_{ij} = \frac{a}{R^m} \left( \frac{1}{p_{ij}} \right) - K \frac{q^2}{R} \left( \frac{\mp 1}{p_{ij}} \right)$$

(8.3)

: (8.3) j

$$(9.3) U_i = \sum_{i(j\neq i)} U_{ij} = \frac{a}{R^m} A_n - |\alpha| K \frac{q^2}{R}$$

:

(10.3) 
$$A_n = \sum_{j(j \neq i)} \left(\frac{1}{p_{ij}}\right)^n$$

(11.3) 
$$\alpha = \sum_{j(j\neq i)} \left(\frac{\mp 1}{p_{ij}}\right)$$

(Madelung)  $\alpha$  m  $A_n$ 

: 2*N* 

(12.3) 
$$U_{tot}(R) = \left(\frac{1}{2}\right) 2NU_i = N\left(\frac{a}{R^m}A_n - |\alpha|\frac{Kq^2}{R}\right)$$

. 1/2

 $R_0$ 

الروابط البلوسة واكخصائص المرونية

(13.3) 
$$\left(\frac{dU_{tot}(R)}{dR}\right)_{R_0} = 0$$

$$N\left(\frac{-ma}{R_0^{m+1}}A_n + |\alpha|\frac{Kq^2}{R_0^2}\right) = 0$$

(14.3) 
$$R_0 = \left(\frac{m a A_n}{|\alpha| K q^2}\right)^{\frac{1}{m-1}}$$

: 
$$(R = R_0) (12.3) (14.3)$$

(15.3) 
$$U_{tot}(R_0) = -|\alpha| \frac{NKq^2}{R_0} \left(1 - \frac{1}{m}\right)$$

) 
$$\frac{U_{tot}(R_0)}{N} = -|\alpha| \frac{Kq^2}{R_0} \left(1 - \frac{1}{m}\right) \qquad \left(-|\alpha| \frac{NKq^2}{R_0}\right)$$

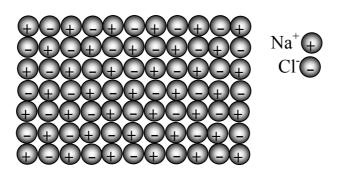
$$N_a \qquad . \qquad ($$

$$. \qquad (J/mole)$$

طاقة الالتحام (mole/ K.J)	البلورة	طاقة الالتحام (mole/ K.J)	البلورة
635	بروميد الروبيديوم RbBr	752	كلوريد الصوديوم NaCl
595	أيوديد السيزيوم <i>CsI</i>	650	أيوديد البوتاسيوم KI

الجدول (1.3):

: (100)



الشكل(2.3):

مثال:

الشكل(3.3):

(16.3) 
$$\left| \alpha \right| = \left| \sum_{j(j \neq i)} \left( \frac{\mp 1}{p_{ij}} \right) \right| = \left| \sum_{j(j \neq i)} \left( \frac{\mp 1}{\left( \frac{r_{ij}}{R} \right)} \right) \right| = \left| \sum_{j(j \neq i)} \left( \frac{\mp R}{r_{ij}} \right) \right|$$

$$\left|\alpha\right| = \left|\sum_{j(j\neq i)} \left(\frac{\mp 1}{p_{ij}}\right)\right| = 2\left(1 - \frac{1}{2} + \frac{1}{3} - \frac{1}{4} + \frac{1}{5} - \dots\right)$$

: 0 ln(1+x)

$$\ln(1+x) = \left(x - \frac{x^2}{2} + \frac{x^3}{3} - \frac{x^4}{4} + \frac{x^5}{5} - \dots\right)$$

$$\ln(1+1) = \ln(2) = \left(1 - \frac{1}{2} + \frac{1}{3} - \frac{1}{4} + \frac{1}{5} - \dots\right)$$

```
(17.3) |\alpha| = |2(\ln(2))| = 1.3863
```

					البنية البلورية
1.638	1.762	1.747	1.792	1.792	ثابت مادلونغ

الجدول (2.3):

#### 3-4 الرابطة التساهمية:

)
((
(14 $SI^{28}$ )
(15 $^2$ 28 $^2$ 2P $^6$ 3S $^2$ 3P $^2$ )
(15 $^2$ 28 $^2$ 2P $^6$ 3S $^2$ 3P $^2$ )
(4.3)

96

(5.3)

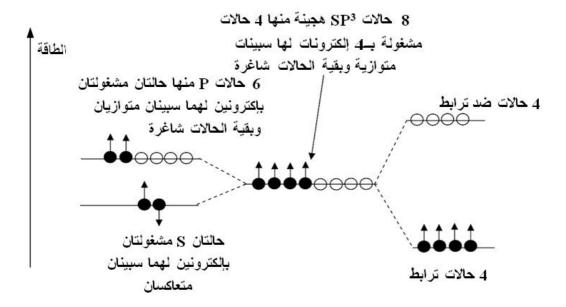
( )  $SP^3$ 

 $SP^3$ 

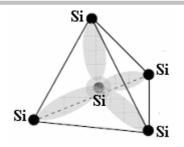
,

.1

.2



الشكل(4.3):



الشكل(5.3):

(3.3)

$\binom{\circ}{C}$ درجة حرارة الانصهار	طاقة الالتحام (KJ/ mole)	البلورة
1410	713	الماس C
>3550	450	سيلكون Si
*	3.5	جرمانيوم Ge

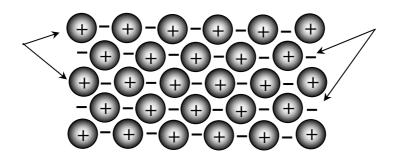
الجدول (3.3):

3-5 الرابطة المعدنية:

.((6.3)

98 °C

 $\cdot 660 \, ^{\circ}C$  650  $^{\circ}C$ 



الشكل (6.3): مخطط مبسط للرابطة المعدنية

(4.3)

درجة حرارة الانصهار (°C)	طاقة الالتحام (KJ / mole)	بلورة
660	324	الألمنيوم Al
1538	406	الحديد Fe
3410	849	التنفستن W

الجدول (4.3):

# 6-3 رابطة فان درفالس (Van Der Waals) أوالرابطة الجزيئية:

0.2**ev** 

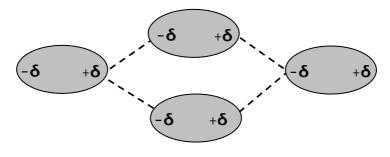
(London) 1930

```
(Heisenberg)
)
.(
,((7.3) )
```

•

)

CFC .( $Xe(-112^{\circ}C)$   $Kr(-156^{\circ}C)$   $Ar(-189^{\circ}C)$   $Ne(-249^{\circ}C)$ 



الشكل(7.3):

درجة حرارة الانصهار (° C)	طاقة الالتحام (KJ / mole)	البلورة
-189	7.7	الأرغون Ar
-101	31	$CL_2$
-78	35	NH <sub>3</sub>

الجدول(5.3):

- j j i

: (Lennard-Jones)

(18.3) 
$$U_{ij}(r_{ij}) = 4\varepsilon \left[ \left( \frac{\sigma}{r_{ij}} \right)^{12} - \left( \frac{\sigma}{r_{ij}} \right)^{6} \right]$$

.  $arepsilon \; \sigma$  :

(19.3) 
$$U_{tot}(R) = \frac{N}{2} \sum_{j(j \neq i)} U_{ij}(r_{ij}) = 2N\varepsilon \left[ \left(\frac{\sigma}{R}\right)^{12} A_{12} - \left(\frac{\sigma}{R}\right)^{6} A_{6} \right]$$

$$: R p_{ij} = \frac{r_{ij}}{R} A_n = \sum_{i \neq j} \left(\frac{1}{p_{ij}}\right)^n :$$

:  $R_0$ 

(20.3) 
$$\left(\frac{dU_{tot}(R)}{dR}\right)_{R_0} = 0 \Rightarrow R_0 = \sigma \left(\frac{2A_{12}}{A_6}\right)^{\frac{1}{6}}$$

: 
$$(R = R_0) (19.3) (20.3)$$

(21.3) 
$$U_{tot}(R_0) = -\frac{2N\varepsilon\sigma^6 A_6}{2} R_0^{-6} = \frac{N\varepsilon A_6^2}{2A_{12}}$$

$$\frac{U_{tot}(R_0)}{N} = \frac{\varepsilon A_6^2}{2A_{12}}$$

$$A_6 A_{12}$$
 (6.3)

 $A_{12} < A_6$ 

CFC	CC	CS	$A_n$
14.45	12.25	8.40	$A_6$
12.13	9.11	6.20	$A_{12}$

3

تطبيق:

a N CFC

. R

: ( )

(22.3)  $B=V_0 \left(\frac{d^2 U_{tot}}{dV^2}\right)_{T,V_0} = \left(V \frac{d^2 U_{tot}}{dR^2} \left(\frac{dR}{dV}\right)^2\right)_{T,R_0}$ 

.  $V_{\scriptscriptstyle 0}$  :

 $R = \frac{a}{\sqrt{2}} \qquad V = \frac{a^3}{4} N : \qquad CFC$ 

:  $R_0$ 

(23.3)  $R_0 = \sigma \left(\frac{2A_{12}}{A_6}\right)^{\frac{1}{6}} = 1.09\sigma$ 

(24.3)  $V = \frac{a^3}{4} N = \frac{N}{\sqrt{2}} R^3$ 

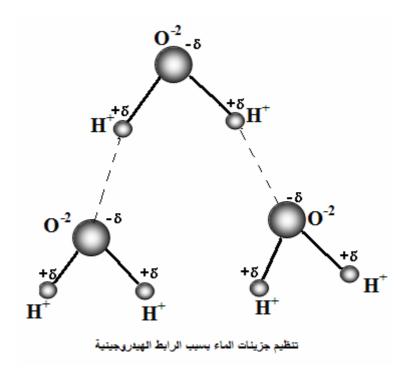
: (24.3) (23.3) (22.3) (22.3)

(25.3)  $B \approx 75 \varepsilon / \sigma^3$ 

6-3 الرابطة الهيدروجينية:

.

(8.3)



الشكل(8.3):

(O---H)

 $(+\delta)$   $(-\delta)$ 

$$(R_{o...H} = 2.76 \text{ A})$$
 .  $(R_{o-H} = 0.96 \text{ A})$ 

ملاحظة عامة:

 $Al_3Li$ 

 $Al_3Li$ 

1.5

Al

1 *Li* 

1.5 V

 $Al_3V$ 

3-9 الخصائص المرونية:

( )

3-9-1 قانون هوك(Hooke):

(1.3) U(R)A

(28.3)

 $U(R_0)$ 

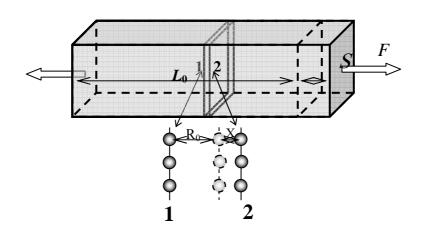
3

لروابط البلومرية واكخصائص المرونية

 $L_0$  S

 $X: \qquad \Delta L = \sum X$ 

.(9.3) 2 1



الشكل (9.3):

:  $F_{\mathrm{int}}$ 

 $(30.3) F_{\rm int} = fN = N\beta X$ 

. S

(31.3) 
$$\sigma = \frac{F_{\text{int}}}{S} = \frac{N\beta X}{S} = CX$$

 $C = \frac{N\beta}{S}$ :

:  $R_0$  (31.3)

(32.3) 
$$\sigma = R_o C \frac{X}{R_o} = \frac{R_o N \beta}{S} \left( \frac{X}{R_o} \right)$$

$$(32.3) E = \frac{R_0 N \beta}{S}, \varepsilon' = \frac{X}{R_0} :$$

$$\sigma = E \varepsilon'$$

$$F R_0 ($$

$$\vdots \varepsilon' L_0 N'+1$$

$$\varepsilon' = \frac{N'X}{N'R_0} = \frac{\Delta L}{L_0} = \varepsilon$$

$$\vdots (33.3)$$

$$(35.3) \sigma = E \varepsilon$$

. (Hooke) (35.3)  $\sigma = E \qquad \varepsilon = 1 \qquad (35.3)$ 

(7.3)

•

E (1	المادة	
النهاية الصغرى		
64	77	Al
68	194	Cu
135	290	Fe
437	514	Mg
400	400	W

الجدول (7.3): معامل يونغ لبعض المعادن.

#### 3-9-3 منحنى الإجماد والانفعال:

.(10.3) 
$$\sigma_e \qquad \qquad : \mathbf{OA} \$$
المجال  $\sigma_e \qquad \qquad . \ (\sigma \propto \varepsilon)$ 

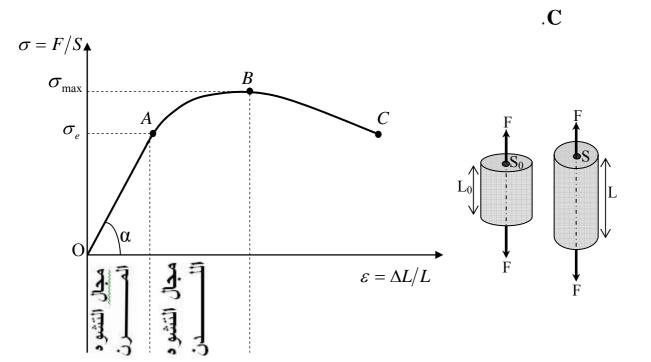
$$\begin{array}{ll} \sigma = 0 \Rightarrow \varepsilon = 0 \\ \sigma \neq 0 \Rightarrow \sigma = \tan{(\alpha)}\varepsilon \Rightarrow E = \tan{(\alpha)} \end{array}$$
 
$$\begin{array}{ll} \sigma > \sigma_e \end{array} \qquad \qquad : \textbf{AB}$$
 المجال

· ·

:

(37.3)  $\sigma = \Gamma \varepsilon^{m}$   $\vdots m \qquad \Gamma :$ 

)  $\sigma_{
m max}$  :BC المجال



الشكل (10.3) المنحنى الاسمي إجهاد - انفعال.

### 3-9-3 معامل بواسون والانفعال الحجمي:

.

(11.3) 
$$(XYZ)$$
  $(YYZ)$   $(YYZ)$ 

.( ) 
$$Z X \qquad \varepsilon_Z \varepsilon_x$$
 : (34.3)

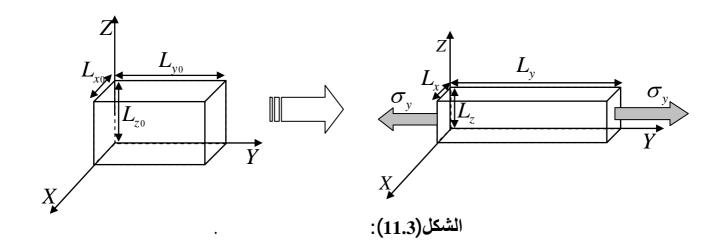
(38.3) 
$$\varepsilon_{y} = \frac{\Delta L_{y}}{L_{y0}} = \frac{L_{y} - L_{y0}}{L_{y0}} > 0$$

(39.3) 
$$\varepsilon_{x} = \frac{\Delta L_{x}}{L_{x0}} = \frac{L_{x} - L_{x0}}{L_{x0}} < 0$$

(40.3) 
$$\varepsilon_{y} = \frac{\Delta L_{z}}{L_{z0}} = \frac{L_{z} - L_{z0}}{L_{z0}} < 0$$

ν

(41.3) 
$$v = -\frac{\varepsilon_x}{\varepsilon_y} = -\frac{\varepsilon_Z}{\varepsilon_y}$$



. (8.3)

المطاط	النحاس	الفولاذ	المادة
0.5	0.36	0.25	معامل بواسون

الجدول(8.3):

$$:\frac{\Delta V}{V_0}$$
 (

$$(42.3) V_0 = L_{x0} \times L_{y0} \times L_{z0} V = L_x \times L_y \times L_z$$

(43.3) 
$$\varepsilon_{x} = \frac{L_{x} - L_{x0}}{L_{x0}} \Rightarrow L_{x} = L_{x0} (1 + \varepsilon_{x})$$

:

$$(44.3) L_{y} = L_{y0} (1 + \varepsilon_{y})$$

$$(45.3) L_z = L_{z0} (1 + \varepsilon_z)$$

:

$$V = L_{x0} (1 + \varepsilon_x) \times L_{y0} (1 + \varepsilon_y) \times L_{z0} (1 + \varepsilon_z) = V_0 ((1 + \varepsilon_x) \times (1 + \varepsilon_y) \times (1 + \varepsilon_z))$$

$$\frac{\Delta V}{V_0} = \frac{V - V_0}{V_0} = ((1 + \varepsilon_x) \times (1 + \varepsilon_y) \times (1 + \varepsilon_z) - 1)$$

$$\frac{\Delta V}{V_0} = \varepsilon_x + \varepsilon_y + \varepsilon_z = \sum_{i=1}^3 \varepsilon_i$$

$$(46.3)$$

 $\varepsilon_x \varepsilon_y \approx \varepsilon_x \varepsilon_z \approx \varepsilon_y \varepsilon_z \approx \varepsilon_x \varepsilon_y \varepsilon_z \approx 0$ :

(46.3) (41.3)

$$\frac{\Delta V}{V_0} = \varepsilon_y (1 - 2\nu)$$

r L

(48.3) 
$$v = -\frac{\varepsilon_r}{\varepsilon_L} = -\frac{\Delta r/r_0}{\Delta L/L_0}$$

$$V = L\pi r^2 \Rightarrow \frac{\Delta V}{V_0} = \frac{\Delta L}{L_0} + 2\frac{\Delta r}{r_0}$$

$$\frac{\Delta V}{V_0} = \varepsilon_L (1 - 2\nu)$$
 :

#### 3-9-3 معامل القص:

τ

τ .(12.3) *θ* 

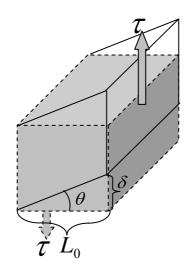
:  $\gamma$ 

(50.3)  $\gamma = \tan(\theta) = \frac{\delta}{L_0}$ 

 $: \qquad \qquad \tau \propto \gamma \qquad \qquad \theta$ 

(51.3)  $\gamma \cong \theta(radian) \cong \frac{\delta}{L_0}$ 

.  $\gamma$ 



الشكل (12.3):تأثير إجهاد القص

. (9.3)

Е (	المادة	
النهاية الصغرى		
25	29	Al
31	77	Cu
61	180	Fe
171	184	Mg
155	155	W

الجدول (9.3):

علاحظة:

$$G = \frac{E}{2(1+\nu)}$$

#### 3-9-3 ممتد الإجماد:

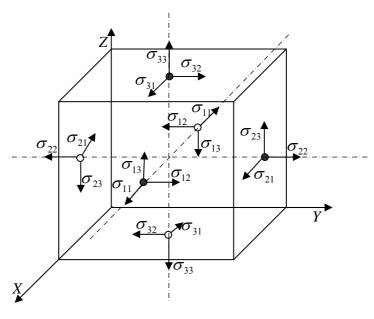
$$\begin{bmatrix} \sigma_{ij} \end{bmatrix}$$

$$i \qquad .((13.3) \qquad )$$

$$j \qquad \qquad j$$

.

(54.3) 
$$\left[\sigma_{ij}\right] = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{pmatrix}$$



الشكل(13.3):

#### 1. خصائص محتد الإجهاد:

9 
$$(i \neq j) \qquad \sigma_{ij} = \sigma_{ji}$$

(55.3) 
$$\left[ \sigma_{ij} \right] = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & \sigma_{33} \end{pmatrix}$$

(56.3) 
$$\det([\sigma_{ij}] - \mu I) = \begin{vmatrix} \sigma_{11} - \mu & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \mu & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & \sigma_{33} - \mu \end{vmatrix} = 0$$

 $\mu_3, \mu_2, \mu_1$ 

:  $\sigma_3, \sigma_2, \sigma_1$ 

(57.3) 
$$[\sigma] = \begin{pmatrix} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{pmatrix}$$

 $\sum^{-}(O', x'_1, x'_2, x'_3) \qquad \qquad \sum (O, x_1, x_2, x_3)$ 

:

(58.3) 
$$\sigma_{ij} = \sum_{k,l=1}^{3} a_{ik} a_{jl} \sigma_{kl} \qquad i, j = 1,2,3$$

 $\sum (O, x_1, x_2, x_3) \qquad \qquad \vdots a_{ik}, a_{jl} :$ 

.  $\sum^{-}(O', x'_1, x'_2, x'_3)$ 

 $: \vec{T}(M, \vec{n})$ عساب شعاع الإجهاد الكلي 2.

 $\vec{n}$  M  $\vec{T}(M,\vec{n})$ 

 $\vec{n}$ 

(59.3) 
$$\vec{T}(M,\vec{n}) = \left[\sigma_{ii}\right] \cdot \vec{n}$$

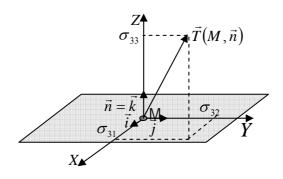
 $T_t$   $T_n$ 

الروابط البلومرية واكخصائص المرونية

3

(60.3) 
$$T_{n} = \vec{T}(M, \vec{k}) \cdot \vec{n}$$
$$T_{t} = \sqrt{(\vec{T}(M, \vec{k}))^{2} - (T_{n})^{2}}$$

 $\vec{k}$  :(14.3)



 $\vec{k}$ 

الشكل(14.3):

$$(i \neq j) \, \sigma_{ij} = \sigma_{ji}$$

$$\vec{T}(M,\vec{k}) = \sigma_{31}\vec{i} + \sigma_{32}\vec{j} + \sigma_{33}\vec{k} = \sigma_{13}\vec{i} + \sigma_{23}\vec{j} + \sigma_{33}\vec{k}$$

$$\vec{T}(M,\vec{k}) = \begin{bmatrix} \sigma_{ij} \end{bmatrix} \cdot \vec{k} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & \sigma_{33} \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} = \begin{pmatrix} \sigma_{13} \\ \sigma_{23} \\ \sigma_{33} \end{pmatrix} = \sigma_{13} \vec{i} + \sigma_{23} \vec{j} + \sigma_{33} \vec{k}$$

 $T_t$ 

(61.3) 
$$T_n = \vec{T}(M, \vec{k}) \cdot \vec{k} = \sigma_{33}$$

(62.3) 
$$T_{t} = \sqrt{\left(\vec{T}(M,\vec{k})\right)^{2} - \left(T_{n}\right)^{2}} = \sqrt{\left(\sigma_{13}^{2} + \sigma_{23}^{2} + \sigma_{33}^{2}\right) - \sigma_{33}^{2}} = \sqrt{\sigma_{13}^{2} + \sigma_{23}^{2}}$$

3-9-3 معامل الانضغاط الحجمي:

 $\Delta p$ 

 $A_0$ 

 $P_0$ 

F

3

 $P_0$ + $\Delta p$ 

 $-\Delta p$ 

(15.3)

:

(63.3)  $\sigma_{ij} = -\Delta p \, \delta_{ij}$ 

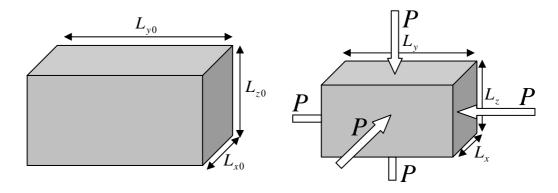
.  $\delta_{ij}$  :

В

 $\Delta P$ 

 $\frac{\Delta V}{V_0}$ 

(64.3)  $B = -\frac{\Delta p}{\left(\frac{\Delta V}{V}\right)}$ 



الشكل (15.3):

: *χ* 

(65.3) 
$$\chi = \frac{1}{B} = -V_0 \frac{\Delta V}{\Delta P}$$

## 3-9-7 ممتد الانفعال:

 $x_i' \quad x_i$ 

:

(66.3) 
$$u_i = x'_i - x_i = \sum_{j=1}^{3} \zeta_{ij} x_j \quad i = 1,2,3$$

:  $\left[\mathcal{L}_{ij}\right]$ 

(67.3) 
$$\left[\zeta_{ij}\right] = \begin{pmatrix} \zeta_{11} & \zeta_{12} & \zeta_{13} \\ \zeta_{21} & \zeta_{22} & \zeta_{23} \\ \zeta_{31} & \zeta_{32} & \zeta_{33} \end{pmatrix}$$

:

$$(i \neq j) \qquad \zeta_{ij} = \partial u_i / \partial x_j \qquad \qquad [\zeta_{ij}]$$

$$.ox_j \qquad ox_i \qquad ox_k$$

$$ox_i \qquad ( )$$

•

(68.3) 
$$\left[ \zeta_{ij} \right] = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} & \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_2}{\partial x_2} \\ \frac{\partial u_3}{\partial x_1} & \frac{\partial u_3}{\partial x_2} & \frac{\partial u_3}{\partial x_3} \end{pmatrix}$$

 $\left[arsigma_{ij}
ight]$ 

:

(69.3) 
$$\zeta_{ij} = \varpi_{ij} + \varepsilon_{ij} \qquad i, j = 1,2,3$$

 $\left[\omega_{ij}
ight]$ 

: 0

(70.3) 
$$\varpi_{ij} = \frac{1}{2} (\zeta_{ij} - \zeta_{ji}) = -\frac{1}{2} (\zeta_{ji} - \zeta_{ij}) = -\varpi_{ji}$$
  $i, j = 1, 2, 3$ 

:  $\left[ \omega_{ij} \right]$ 

(71.3) 
$$\left[ \boldsymbol{\varpi}_{ij} \right] = \begin{pmatrix} 0 & \boldsymbol{\varpi}_{12} & \boldsymbol{\varpi}_{13} \\ -\boldsymbol{\varpi}_{12} & 0 & \boldsymbol{\varpi}_{23} \\ -\boldsymbol{\varpi}_{13} & -\boldsymbol{\varpi}_{23} & 0 \end{pmatrix}$$

6

(72.3) 
$$\left[ \boldsymbol{\varpi}_{ij} \right] = \begin{pmatrix} 0 & \frac{1}{2} \left( \frac{\partial u_1}{\partial x_2} - \frac{\partial u_2}{\partial x_1} \right) & \frac{1}{2} \left( \frac{\partial u_1}{\partial x_3} - \frac{\partial u_3}{\partial x_1} \right) \\ -\frac{1}{2} \left( \frac{\partial u_1}{\partial x_2} - \frac{\partial u_2}{\partial x_1} \right) & 0 & \frac{1}{2} \left( \frac{\partial u_2}{\partial x_3} - \frac{\partial u_3}{\partial x_2} \right) \\ -\frac{1}{2} \left( \frac{\partial u_1}{\partial x_3} - \frac{\partial u_3}{\partial x_1} \right) & -\frac{1}{2} \left( \frac{\partial u_2}{\partial x_3} - \frac{\partial u_3}{\partial x_2} \right) & 0 \end{pmatrix}$$

 $\left[ {{oldsymbol{arepsilon }}_{ij}} 
ight]$ 

(73.3) 
$$\varepsilon_{ij} = \frac{1}{2} \left( \zeta_{ij} + \zeta_{ji} \right) = \frac{1}{2} \left( \zeta_{ji} + \zeta_{ij} \right) = \varepsilon_{ji} \qquad i, j = 1,2,$$

:  $\left[ \mathcal{E}_{ij} \right]$ 

$$\begin{bmatrix} \boldsymbol{\varepsilon}_{ij} \end{bmatrix} = \begin{pmatrix} \boldsymbol{\varepsilon}_{11} & \boldsymbol{\varepsilon}_{12} & \boldsymbol{\varepsilon}_{13} \\ \boldsymbol{\varepsilon}_{12} & \boldsymbol{\varepsilon}_{22} & \boldsymbol{\varepsilon}_{23} \\ \boldsymbol{\varepsilon}_{13} & \boldsymbol{\varepsilon}_{23} & \boldsymbol{\varepsilon}_{33} \end{pmatrix}$$

(74.3) 
$$\left[ \varepsilon_{ij} \right] = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{1}{2} \left( \frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right) & \frac{1}{2} \left( \frac{\partial u_1}{\partial x_3} + \frac{\partial u_3}{\partial x_1} \right) \\ \frac{1}{2} \left( \frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right) & \frac{\partial u_2}{\partial x_2} & \frac{1}{2} \left( \frac{\partial u_2}{\partial x_3} + \frac{\partial u_3}{\partial x_2} \right) \\ \frac{1}{2} \left( \frac{\partial u_1}{\partial x_3} + \frac{\partial u_3}{\partial x_1} \right) & \frac{1}{2} \left( \frac{\partial u_2}{\partial x_3} + \frac{\partial u_3}{\partial x_2} \right) & \frac{\partial u_3}{\partial x_3} \end{pmatrix}$$

 $igl[arepsilon_{ij}igr]$ 

3-9-3 قانون هوك المعمم:

1) حالة المواد موحدة الخواص (متماثلة المناحي):

:

,  $\sigma_{ii}$  ( )

(

V E .

: (35.3)

(75.3)  $\sigma = E\varepsilon \Rightarrow \varepsilon = \frac{\sigma}{F}$ :

 $: \mathcal{E}_{11}$ 

(76.3) 
$$\varepsilon_{11} = \frac{\sigma_{11}}{E} - v \frac{\sigma_{22}}{E} - v \frac{\sigma_{33}}{E}$$
$$\varepsilon_{11} = \frac{1}{E} (\sigma_{11} - v (\sigma_{22} + \sigma_{33}))$$

:  $\mathcal{E}_{33}$  ,  $\mathcal{E}_{22}$ 

(77.3) 
$$\varepsilon_{22} = \frac{1}{E} (\sigma_{22} - \nu (\sigma_{11} + \sigma_{33}))$$

(78.3) 
$$\varepsilon_{33} = \frac{1}{E} (\sigma_{33} - \nu (\sigma_{11} + \sigma_{22}))$$

: (78.3) ,(77.3) ,(76.3)

(79.3) 
$$\varepsilon_{ii} = \frac{1}{F} (\sigma_{ii} - v\sigma_{11} - v\sigma_{22} - v\sigma_{33} + v\sigma_{ii}) \qquad i = 1, 2, 3$$

(80.3) 
$$\varepsilon_{ii} = \frac{1}{E} \left( (1 + v) \sigma_{ii} - v \operatorname{trac} \left[ \sigma_{ij} \right] \right) \qquad i = 1, 2, 3$$

 $trac\left[\sigma_{ij}\right] = \sigma_{11} + \sigma_{22} + \sigma_{33} :$ 

) 
$$\gamma_{ij} = 2\varepsilon_{ij}(i \neq j)$$
 
$$\tau_{ij} = \sigma_{ij}(i \neq j)$$
 
$$\vdots \qquad (\gamma_{ij})$$

(52.3)

(81.3) 
$$\sigma_{ij} = G\gamma_{ij} = 2G\varepsilon_{ij} \Rightarrow \varepsilon_{ij} = \frac{1}{2G}\sigma_{ij} \qquad i, j = 1,2,3$$

(82.3) 
$$\varepsilon_{ij} = \frac{1}{2\left(\frac{E}{2(1+\nu)}\right)}\sigma_{ij} = \frac{1+\nu}{E}\sigma_{ij} \qquad i, j = 1,2,3$$

: (82.3) (80.3)

(83.3) 
$$\varepsilon_{ij} = \frac{1}{F} ((1+v)\sigma_{ij} - v trac [\sigma_{ij}] \delta_{ij}) \qquad i, j = 1,2,3$$

.  $\delta_{ij}$  :

.

(84.3) 
$$\sigma_{ij} = \frac{E}{1+\nu} \left( \varepsilon_{ij} + \frac{\nu}{1-2\nu} trac \left[ \sigma_{ij} \right] \delta_{ij} \right) \qquad i = 1,2,3$$

 $: \qquad \mu \, , \lambda \qquad \qquad (38.3)$ 

(85.3) 
$$\sigma_{ij} = 2\mu\varepsilon_{ij} + \lambda trac \left[\sigma_{ij}\right] \delta_{ij} \qquad i = 1,2,3$$

: (85.3) (84.3)

$$(86.3) 2\mu = \frac{E}{1+\nu}$$

(87.3) 
$$\lambda = \frac{E \nu}{(1+\nu)(1-2\nu)}$$

E G B :

:  $\nu$ 

3

الروابط البلومرية وانخصائص المرونية

(88.3) 
$$B = -\frac{\Delta p}{\left(\frac{\Delta V}{V}\right)} = -\frac{\Delta p}{\left(\sum_{i=1}^{3} \mathcal{E}_{ii}\right)}$$

.(64.3) (46.3)

: (84.3) (83.3)

(89.3) 
$$\varepsilon_{ii} = \frac{1}{F} ((1+v)\sigma_{ii} - v\sigma_{11} - v\sigma_{22} - v\sigma_{33}) \qquad i = 1,2,3$$

(90.3) 
$$\sum_{i=1}^{3} \varepsilon_{ii} = \sum_{i=1}^{3} \frac{1}{E} ((1+\nu)\sigma_{ii} - \nu\sigma_{11} - \nu\sigma_{22} - \nu\sigma_{33}) \qquad i = 1,2,3$$
$$= \frac{1}{E} ((1-2\nu)(\sigma_{11} + \sigma_{22} + \sigma_{33}))$$

:

(91.3) 
$$\sigma_{ij} = -\Delta p \, \delta_{ij} \qquad i, j = 1,2,3$$
$$\sigma_{ii} = -\Delta p \qquad i = 1,2,3$$

: (90.3) (91.3)

(92.3) 
$$\sum_{i=1}^{3} \varepsilon_{ii} = \frac{-3\Delta p}{E} (1 - 2\nu) \qquad i = 1,2,3$$

: (88.3)

(93.3) 
$$B = \frac{E}{3(1-2\nu)}$$

: (93.3) (53.3) *v* 

(94.3) 
$$B = \frac{GE}{3(3G - E)}$$

:( **(2**  $\left(3^4 = 9 \times 9 = 81\right)$  $\sigma_{ij} = \sum_{k,l=1}^{3} C_{ijkl} \varepsilon_{kl}$   $_{i,j=1,2,3}$ (95.3)  $\varepsilon_{ij} = \sum_{k l=1}^{3} S_{ijkl} \sigma_{kl} \qquad \qquad _{i,j=1,2,3}$ (96.3) (96.3) (95.3) 81  $C_{ijkl}$  $S_{ijkl}$ (9  $(6 \times 6 = 36)$  $S_{ijkl} = S_{klij}$   $C_{ijkl} = C_{klij}$ : ) 21 )) 180°

:

3

الروابط البلومية واكخصائص المرونية

(97.3) 
$$C'_{ijkl} = \sum_{m,n,p,q=1}^{3} a_{im} a_{jn} a_{kp} a_{lq} C_{mnpq} \qquad _{i,j,k,l=1,2,3}$$

(98.3) 
$$S'_{ijkl} = \sum_{m,n,p,q=1}^{3} a_{im} a_{jn} a_{kp} a_{lq} S_{mnpq} \qquad _{i,j,k,l=1,2,3}$$

 $x_r$   $x_h'$   $a_{hr}$ 

 $y = S'_{3333}$   $X'_3$  E (98.3)

 $(k \leftrightarrow l) \quad (i \leftrightarrow j)$ 

$$(11 \rightarrow 1) \qquad (23,32 \rightarrow 4)$$

$$(22 \rightarrow 2) \qquad (13,31 \rightarrow 5)$$

$$(33 \rightarrow 3) \qquad (12,21 \rightarrow 6)$$

•

(100.3) 
$$\varepsilon_p = \sum_{g=1}^6 S_{pg} \, \sigma_g \qquad \qquad _{g=1,\dots,6}$$

$$C_{ijkl} = C_{klij}$$
  $C_{pg} = C_{gp}$  ((100.3) ) (99.3)

.

الروابط البلومرية واكخصائص المرونية

6

$$\begin{pmatrix}
\sigma_{1} \\
\sigma_{2} \\
\sigma_{3} \\
\sigma_{4} \\
\sigma_{5} \\
\sigma_{6}
\end{pmatrix} = \begin{pmatrix}
C_{11} & C_{12} & C_{13} & C_{14} & C_{15} & C_{16} \\
C_{12} & C_{22} & C_{23} & C_{24} & C_{25} & C_{26} \\
C_{13} & C_{23} & C_{33} & C_{34} & C_{35} & C_{36} \\
C_{14} & C_{24} & C_{34} & C_{44} & C_{45} & C_{46} \\
C_{15} & C_{25} & C_{35} & C_{45} & C_{55} & C_{56} \\
C_{16} & C_{26} & C_{36} & C_{46} & C_{56} & C_{66}
\end{pmatrix} \times \begin{pmatrix}
\varepsilon_{1} \\
\varepsilon_{2} \\
\varepsilon_{3} \\
\varepsilon_{4} \\
\varepsilon_{5} \\
\varepsilon_{6}
\end{pmatrix}$$

تطبيق: 3

.

:

(102.3) 
$$B = -\frac{\Delta p}{\left(\frac{\Delta V}{V}\right)} = -\frac{\Delta p}{\left(\sum_{i=1}^{3} \varepsilon_{ii}\right)}$$

(103.3) 
$$\sum_{i=1}^{3} \varepsilon_{ii} = \sum_{i=1}^{3} \sum_{k,l=1}^{3} S_{iikl} \sigma_{kl}$$

: (103.3) (91.3)

(104.3) 
$$\sum_{i=1}^{3} \varepsilon_{ii} = \sum_{i=1}^{3} \sum_{k=1}^{3} S_{iikk} \sigma_{kk}$$
$$= -\Delta p \sum_{i,k=1}^{3} S_{iikk}$$

: (102.3) (104.3)

(105.3) 
$$B = \left(\sum_{i,k=1}^{3} S_{iikk}\right)^{-1}$$

• تحدید عناصر همتد ثوابت أو معاملات المرونة:

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.(10.3)

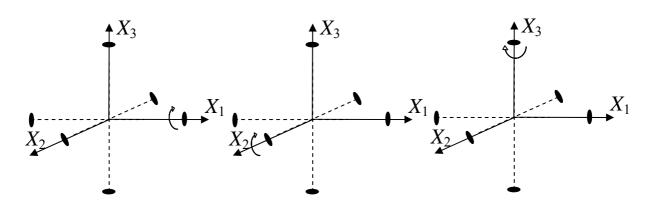
عدد العناصر المستقلة $\mathrm{C}_{\mathtt{pg}}$	الفئة البلورية
21	ثلاثية الميل
31	أحادية الميل
09	المعينية المستقيمة
6	ثلاثية متساوية الأحرف
5	السداسية
3	المكعبة
2	المواد موحدة الخواص

الشكل(10.3): لمتدات

129

2 2 2 m m m

:180°



$$X_{1} \rightarrow X_{1}(1 \rightarrow 1)$$

$$X_{2} \rightarrow -X_{2}(2 \rightarrow \overline{2})$$

$$X_{3} \rightarrow -X_{3}(3 \rightarrow \overline{3})$$

$$\{O_{3}\}$$

$$X_{1} \rightarrow -X_{1}(1 \rightarrow \overline{1})$$

$$X_{2} \rightarrow X_{2}(2 \rightarrow 2)$$

$$X_{3} \rightarrow -X_{3}(3 \rightarrow \overline{3})$$

$$\{O_{2}\}$$

$$X_{1} \rightarrow -X_{1}(1 \rightarrow \overline{1})$$

$$X_{2} \rightarrow X_{2}(2 \rightarrow 2)$$

$$X_{3} \rightarrow -X_{3}(3 \rightarrow \overline{3})$$

$$\{O_{2}\}$$

$$X_{1} \rightarrow -X_{1}(1 \rightarrow \overline{1})$$

$$X_{2} \rightarrow -X_{2}(2 \rightarrow \overline{2})$$

$$X_{3} \rightarrow X_{3}(3 \rightarrow 3)$$

$$\{O_{1}\}$$

$$ijkl$$
  $\left[C_{ijkl}\right]$ 

$$[A] = \begin{pmatrix} 1111 & 1122 & 1133 & 1123 & 1131 & 1112 \\ & 2222 & 2233 & 2223 & 2231 & 2212 \\ & & 3333 & 3323 & 3331 & 3312 \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & \\ & & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & \\ & & & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & \\ & & &$$

: [B]

$$.[B] \qquad \qquad \{O_1\} \qquad \qquad [A]$$

 $3323 \xrightarrow{o_1} 33\overline{2}3 = -3323$ 

 $3131 \xrightarrow{O_1} 3\overline{1}3\overline{1} = 3131$ 

 $2223 \xrightarrow{o_1} \overline{2223} = -2223$ 

 $1112 \xrightarrow{o_1} \overline{1} \overline{1} \overline{1} \overline{2} = 1112$ 

 $3333 \xrightarrow{O_1} 3333$ 

.

$$[B] = \begin{pmatrix} 1111 & 1122 & 1133 & -1123 & -1131 & 1112 \\ & 2222 & 2233 & -2223 & -2231 & 2212 \\ & & 3333 & -3323 & -3331 & 3312 \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\$$

[B] = [A]

$$[B][A]$$

$$(3331 \rightarrow -3331 \Leftrightarrow C_{3331} \rightarrow -C_{3331} \Rightarrow C_{3331} = 0)$$

$$\cdot [D] [B]$$

$$[D] = \begin{pmatrix} 1111 & 1122 & 1133 & 0 & 0 & 1112 \\ & 2222 & 2233 & 0 & 0 & 2212 \\ & & 3333 & 0 & 0 & 3312 \\ & & & 2323 & 2331 & 0 \\ & & & & & 3131 & 0 \\ & & & & & & & 1212 \end{pmatrix}$$

$$[E] = \begin{bmatrix} 0 & 0 & 0 & -1112 \\ 1111 & 1122 & 1133 & 0 & 0 & -1112 \\ 2222 & 2233 & 0 & 0 & -2212 \\ 3333 & 0 & 0 & -3312 \\ 2323 & -2331 & 0 \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ &$$

 $O_3$  .

[E] .

•

(106.3) 
$$\left[ C_{ij} \right] = \begin{pmatrix} C_{11} & C_{12} & C_{13} & 0 & 0 & 0 \\ C_{12} & C_{22} & C_{23} & 0 & 0 & 0 \\ C_{13} & C_{23} & C_{33} & 0 & 0 & 0 \\ 0 & 0 & 0 & C_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & C_{55} & 0 \\ 0 & 0 & 0 & 0 & 0 & C_{66} \end{pmatrix}$$

:

$$C_{44}, C_{12}, C_{11}$$
 :

(107.3) 
$$\left[ C_{ij} \right] = \begin{pmatrix} C_{11} & C_{12} & C_{12} & 0 & 0 & 0 \\ C_{12} & C_{11} & C_{12} & 0 & 0 & 0 \\ C_{12} & C_{12} & C_{11} & 0 & 0 & 0 \\ 0 & 0 & 0 & C_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & C_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & C_{44} \end{pmatrix}$$

$$C_{44}, C_{12}, C_{13}, C_{33}, C_{11}$$
 : (2

(108.3) 
$$\begin{bmatrix} C_{1j} \end{bmatrix} = \begin{pmatrix} C_{11} & C_{12} & C_{13} & 0 & 0 & 0 \\ C_{12} & C_{11} & C_{13} & 0 & 0 & 0 \\ C_{13} & C_{13} & C_{33} & 0 & 0 & 0 \\ 0 & 0 & 0 & C_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & C_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{1}{2} (C_{11} - C_{12}) \end{pmatrix}$$

$$C_{12}, C_{11}$$
 :

(109.3) 
$$[C_{ij}] = \begin{pmatrix} C_{11} & C_{12} & C_{12} & 0 & 0 & 0 \\ C_{12} & C_{11} & C_{12} & 0 & 0 & 0 \\ C_{12} & C_{12} & C_{11} & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{1}{2}(C_{11} - C_{12}) & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1}{2}(C_{11} - C_{12}) & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{1}{2}(C_{11} - C_{12}) \end{pmatrix}$$

कृं। गी रीजवं॥

# اهتزازات الشبكة البلورية والخصائص الحرارية

#### 1-4 مقدمة

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# 2-4 الخط الدري المتجانس أو الوتر المشدود

a  $\lambda > a$  .(1.4)

 $\left(\omega_{\min} = 2\pi v_{S}/\lambda_{\max}\right) \tag{1.4}$ 

 $.\left(\omega_{\max}=2\pi v_S/\lambda_{\min}=\pi v_S/a\right)$ :  $\left(\lambda_{\min}=2a\right)$ 

:  $v_s$  u

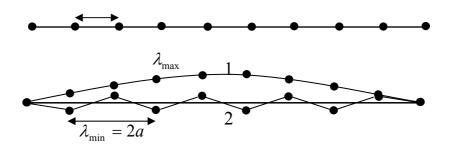
(1.4) 
$$\frac{\partial^2 u}{\partial x^2} = \frac{1}{\mathbf{v}_{\mathrm{S}}^2} \frac{\partial^2 u}{\partial t^2}$$

:  $E \qquad \left(\mathbf{v}_{\mathrm{S}} = \sqrt{E/\rho}\right) :$ 

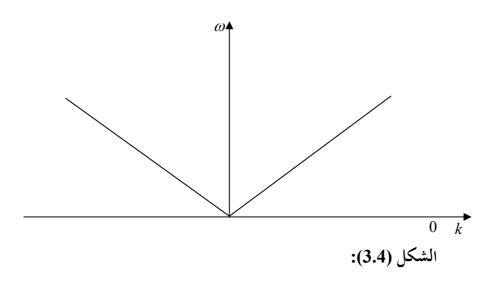
(2.4) 
$$u = u_0 \exp(i(\omega t \pm k x))$$

k  $\omega$  ( , )  $\omega = v_S k$  :  $v_p = v_S$  .(2.4)

.  $V_g$ 



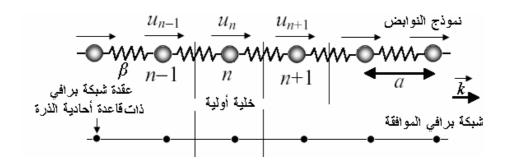
الشكل (1.4):



3-4 أنماط الا له تزاز الطبيعية الشبكة البلورية الخطية المؤلفة من درة واحدة في الخلية لأولية (شبكة برافي الخطية أحاية الدرة)

$$\beta \qquad \qquad (a) \qquad \qquad (m) \qquad \qquad ,$$

$$\beta \qquad \qquad \dots \dots \qquad \qquad .$$



الشكل (3.4):

( ) (3.4) (n) 
$$(...u_{n-1}, u_n, u_{n+1}...)$$

 $\vdots \qquad \qquad n+1 \qquad \qquad n$ 

(3.4) 
$$F_1 = -\beta(u_n - u_{n+1})$$

 $\vdots \hspace{1cm} n\text{-}1 \hspace{1cm} n$ 

(4.4) 
$$F_2 = \beta(u_n - u_{n-1})$$
:  $n$ 

(5.4) 
$$F_n = F_1 - F_2 = -\beta (2u_n - u_{n+1} - u_{n-1})$$
:(3)

$$F_{n} = m\frac{d^{2}u_{n}}{dt^{2}} = m\ddot{u}_{n} = -\beta(2u_{n} - u_{n+1} - u_{n-1})$$

(6.4) 
$$m\ddot{u}_n + \beta(2u_n - u_{n+1} - u_{n-1}) = 0$$

N N (6.4)

 $x_n = na$   $( ) \qquad a$  (3.4)

 $k \qquad \qquad u \qquad \qquad \omega \qquad \qquad ($ 

(7.4)  $u_n = u \exp \left(i(kx_n - \omega t)\right) = u \exp \left(i(nka - \omega t)\right)$ 

 $x_{n-}$   $x_{n+1} = a(n+1)$  (6.4)

:  $_{1}=a(n-1)$ 

 $m\omega^2 = \beta(2 - e^{ika} - e^{-ika})$ 

 $\cos\theta = \frac{1}{2}(e^{i\theta} + e^{-i\theta})$   $\theta = ka$ 

إهتزانرات الشبكة البلومرية وانخصائص انحرامرية

(8.4) 
$$\omega^{2} = \frac{2\beta}{m} (1 - \cos ka) = \frac{4\beta}{m} \sin^{2} \frac{ka}{2}$$

$$\omega = \pm 2\sqrt{\frac{\beta}{m}} \left| \sin \frac{ka}{2} \right|$$

$$\omega = \pm \omega_{\text{max}} \left| \sin \frac{ka}{2} \right|$$

 $\omega_{\text{max}} = 2\sqrt{\beta/m}$ 

(8.4)

### 1-3-4 خصائص علاقة التبدد

$$|\sin ka/2| \qquad \omega(-k) = \omega(k) \qquad \omega(k)$$

$$: \qquad \omega(k) \qquad k' \qquad , \qquad n' \qquad (n'\pi)$$

$$\omega(k) = \omega(k+k') \Rightarrow \qquad |\sin(ka/2)| = |\sin((k+k')a/2)| = |\sin((ka/2) + n'\pi)| \Rightarrow \frac{k'a}{2} = n'\pi \Rightarrow k' = \frac{2\pi n'}{a}$$

$$(8.4) \quad (7.4) \qquad k+2\pi n/a \qquad k \qquad (4.4)$$

 $(k_{max} = \pi/a)$   $2d \sin$   $0 \cos \alpha \cos \alpha$   $\lambda_{min} = 2\pi/k_{max} = 2a$   $\lambda = 2a$   $\lambda = 2a$   $\lambda = 2a$   $0 \cos \alpha \cos \alpha$   $0 \cos$ 

$$(7.4) (k_{\text{max}} = \pm \pi/a)$$

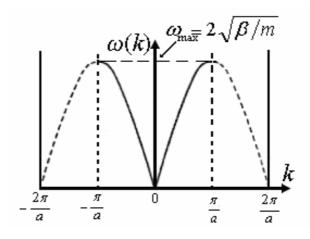
:

(10.4) 
$$u_n = u \exp(\pm in\pi - i\omega t) = (-1)^n u \exp(-i\omega t)$$

n

( )

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الشكل (4.4):

سرعة الطور وسرعة المجموعة

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$$(11.4) V_p = \frac{\omega}{k}$$

: a (11.4) (8.4)

(12.4) 
$$V_{p} = \frac{\omega}{k} = \frac{2\sqrt{\frac{\beta}{m}}\left|\sin\left(\frac{ka}{2}\right)\right|}{k} = \sqrt{\frac{\beta a^{2}}{m}} \cdot \left|\frac{\sin\left(\frac{ka}{2}\right)}{\frac{ka}{2}}\right|$$

 $V_g$ 

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$$(13.4) V_g = \frac{\partial \omega}{\partial k}$$

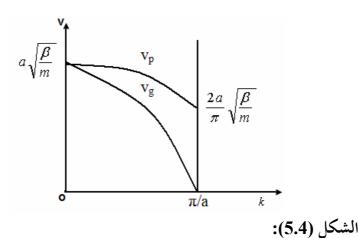
$$V_{g} = \frac{\partial \omega}{\partial k} = \sqrt{\frac{\beta a^{2}}{m}} \left| \cos \left( \frac{ka}{2} \right) \right|$$

$$k = \pm \pi/a \qquad (14.4)$$

$$.\left( (2\pi/a)\sqrt{\beta/m} \right) \qquad (12.4)$$

$$v_{p} \qquad (k = (2\pi/\lambda) \rightarrow 0)$$

$$.(5.4)$$



 $(15.4) \qquad \qquad \sin\left(\frac{ka}{2}\right) = \frac{ka}{2} - \frac{(ka)^3}{3!} + \frac{(ka)^5}{5!} - \dots \approx \frac{ka}{2}$   $(8.4) \qquad (15.4)$ 

(16.4) 
$$\omega = 2\sqrt{\frac{\beta}{m}} \sin\left(\frac{ka}{2}\right) \approx 2\sqrt{\frac{\beta}{m}} \frac{ka}{2} = \sqrt{\frac{\beta a^2}{m}} k$$

(16.4)

(17.4) 
$$\mathbf{v}_p = \mathbf{v}_g = a\sqrt{\frac{\beta}{m}} = \mathbf{v}_S$$

• الشروط الحدية الحدية الدورية لبورن – فون كارمن (Born-von Karmann)

N

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: N

$$(17.4) u_{n\pm N} = u_n$$

: (17.4) (7.4) (discrete)

 $u e^{i(kan \pm kaN - \omega t)} = u e^{i(kan - \omega t)} \Rightarrow$ 

 $\exp(\pm ikaN) = 1 \Rightarrow kaN = 2\pi h \Rightarrow$ 

(18.4) 
$$k = \frac{2\pi}{aN}h = 0, \pm \frac{2\pi}{aN}, \pm \frac{4\pi}{aN}, \pm \frac{6\pi}{aN}..., \pm \frac{N\pi}{aN} = \pm \frac{\pi}{a}$$

(19.4) 
$$-\frac{\pi}{a} \le k \le +\frac{\pi}{a} , -\frac{N}{2} \le h \le +\frac{N}{2}$$

h

.a

) 
$$\left(G=(2\pi/a)n_{g}\right)$$
  $k$  : (a

(20.4) 
$$k' = k + G = k + \frac{2\pi}{a} n_g$$
 (18.4) (7.4) (20.4)

•

## 2-3-4 كثافة الأنماط الا متزازية

(21.4) 
$$g(k) = \frac{1}{\left(\frac{2\pi}{aN}\right)} = \frac{aN}{2\pi}, \quad -\frac{\pi}{a} \le k \le +\frac{\pi}{a}$$

$$\frac{-\pi}{a}$$
  $\frac{-4\pi}{Na} \frac{-2\pi}{Na}$  0  $\frac{2\pi}{Na} \frac{4\pi}{Na}$   $\frac{\pi}{a}$   $\vec{k}$  :(6.4)

(23.4) 
$$g(|k|)dk = 2\frac{aN}{2\pi}dk$$
$$: |k+dk| |k| \qquad k \qquad \omega + d\omega \quad \omega$$

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$$D(\omega)d\omega = g(|k|)dk$$

(24.4) 
$$D(\omega)d\omega = g(|k|)dk = 2\frac{aN}{2\pi}dk$$

 $D(\omega)$ 

(25.4) 
$$D(\omega) = \frac{aN}{\pi} \frac{dk}{d\omega}$$

:

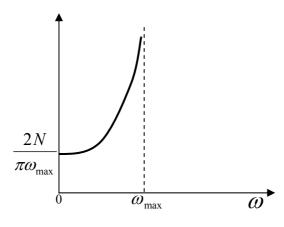
$$\omega = \omega_{\text{max}} \left| \sin \left( \frac{|k|a}{2} \right) \right|$$

$$\frac{d\omega}{dk} = \frac{a\omega_{\text{max}}}{2} \left| \cos\left(\frac{ka}{2}\right) \right| = \frac{a\omega_{\text{max}}}{2} \left(1 - \sin^2\left(\frac{ka}{2}\right)\right)^{\frac{1}{2}}$$
$$= \frac{a}{2} \left(\omega_{\text{max}}^2 - \omega^2\right)^{\frac{1}{2}}$$

:

(26.4) 
$$D(\omega) = \frac{2N}{\pi} (\omega_{\text{max}}^2 - \omega^2)^{-\frac{1}{2}} = \frac{2N}{\pi \omega_{\text{max}}} \left( 1 - \frac{\omega^2}{\omega_{\text{max}}^2} \right)^{-\frac{1}{2}}$$

(7.4)



الشكل (7.4):

$$k \qquad \left[\omega, \omega_{\max}\right] \qquad \omega$$

:

$$\int_{0}^{\omega_{\text{max}}} D(\omega) d\omega = \frac{2N}{\pi} \int_{0}^{\omega_{\text{max}}} \left(\omega_{\text{max}}^{2} - \omega^{2}\right)^{-\frac{1}{2}} d\omega = \frac{2N}{\pi} \left[ \arcsin\left(\frac{\omega}{\omega_{\text{max}}}\right) \right]_{0}^{\omega_{\text{max}}} = \frac{2N}{\pi} \left[\frac{\pi}{2}\right] = N$$

$$(27.4) \qquad \int_{0}^{\omega_{\text{max}}} D(\omega) d\omega = \int_{0}^{\pi/a} g(|k|) dk = \int_{0}^{\pi/a} \frac{aN}{\pi} dk = \frac{aN}{\pi} \left[\frac{\pi}{a}\right] = N$$

4-4 أنماط الا له تزاز الطبيعية الشبكة البلورية الخطية المؤلفة من درتين في الخلية الأولية (شبكة برافي الخطية ثنائية الدرة)

....CsCl, NaCl

....Ge, Si

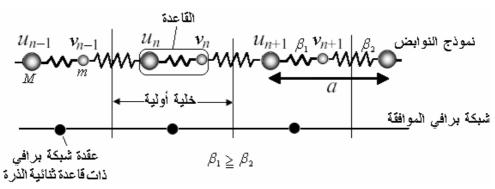
:*N* 

M m  $oldsymbol{eta_1}$ 

.  $\beta_2 \leq \beta_1$   $\beta_2$ 

 $\left(\dots u_{n-1}, u_n, u_{n+1}\dots\right) \qquad M \qquad . \qquad a$ 

 $(...v_{n-1}, v_n, v_{n+1}...) m$ 



الشكل (8.4):

(28.4) 
$$M \ddot{u}_n = -\beta_1 (u_n - v_n) - \beta_2 (u_n - v_{n-1})$$

(29.4) 
$$m\ddot{v}_{n} = -\beta_{1}(v_{n} - u_{n}) - \beta_{2}(v_{n} - u_{n+1})$$
(8.4)

k  $\omega$  (

(30.4) 
$$u_n = u \exp(i(nka - \omega t))$$

(31.4) 
$$v_n = v \exp(i(nka - \omega t))$$

$$v_n \qquad u_n \qquad k \qquad \omega$$

:

: 
$$\exp(iNka) = 1$$
 :  $v_n = v_{n+N} \quad u_n = u_{n+N}$ 

$$k = \frac{2\pi}{aN}h = 0, \pm \frac{2\pi}{aN}, \pm \frac{4\pi}{aN}, \pm \frac{6\pi}{aN}, \dots, \pm \frac{N\pi}{aN} = \pm \frac{\pi}{a}$$
$$-\frac{\pi}{a} \le k \le +\frac{\pi}{a}, -\frac{N}{2} \le h \le +\frac{N}{2}$$

k ( ) : N h:

(29.4) (28.4) (31.4) (30.4) (29.4) (28.4)

<u>.</u>

$$(32.4) \qquad (M\omega^2 - (\beta_1 + \beta_2))u + (\beta_1 + \beta_2 \exp(ika))v$$

(33.4) 
$$(\beta_1 + \beta_2 \exp(ika))u + (m\omega^2 - (\beta_1 + \beta_2))v$$

1 و ٧

(34.4) 
$$\begin{vmatrix} M\omega^2 - (\beta_1 + \beta_2) & \beta_1 + \beta_2 \exp(ika) \\ \beta_1 + \beta_2 \exp(ika) & m\omega^2 - (\beta_1 + \beta_2) \end{vmatrix} = 0$$

:

(35.4) 
$$\omega^{4} - \frac{\beta_{1} + \beta_{2}}{\mu} \omega^{2} + \frac{4\beta_{1}\beta_{2}}{Mm} \sin^{2}\left(\frac{ka}{2}\right) = 0$$

$$m \quad M$$

 $\mu = \frac{Mm}{(M+m)}$  (35.4)

(36.4) 
$$\omega_1^2 = \frac{\beta_1 + \beta_2}{2\mu} \left( 1 - \sqrt{1 - \alpha \sin^2\left(\frac{ka}{2}\right)} \right)$$

(37.4) 
$$\omega_2^2 = \frac{\beta_1 + \beta_2}{2\mu} \left( 1 + \sqrt{1 - \alpha \sin^2\left(\frac{ka}{2}\right)} \right)$$

:

(38.4) 
$$\alpha = 16 \frac{\beta_1 \beta_2}{(\beta_1 + \beta_2)^2} \left(\frac{\mu}{M + m}\right) \le 1$$

$$1-\alpha\sin^2\left(\frac{ka}{2}\right)$$
 :  $M=m$   $\beta_1=\beta_2$ 

 $\omega_2,\omega_1$ 

2N N

 $\omega_2,\omega_1$ 

k

(37.4) . 2N

. (38.4)

•

$$(ka << 1) \quad (\lambda >> a) \tag{3}$$

(38.4) (37.4)

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$$(\sin(ka/2) \approx (ka/2))$$

$$\omega_1^2 = \frac{\beta_1 + \beta_2}{2\mu} \left( 1 - \sqrt{1 - \alpha \left(\frac{ka}{2}\right)^2} \right) \approx \frac{\beta_1 + \beta_2}{2\mu} \left( 1 - \left( 1 - \alpha \left(\frac{1}{2}\right) \frac{k^2 a^2}{4} \right) \right) \Rightarrow$$

149

(39.4) 
$$\omega_1 = \frac{\sqrt{\alpha(\beta_1 + \beta_2)}}{4\sqrt{\mu}} ak$$

$$\omega_{2}^{2} = \frac{\beta_{1} + \beta_{2}}{2\mu} \left( 1 + \sqrt{1 - \alpha \left( \frac{ka}{2} \right)^{2}} \right) \approx \frac{\beta_{1} + \beta_{2}}{2\mu} \left( 1 + \left( 1 - \alpha \frac{k^{2}a^{2}}{8} \right) \right) \Rightarrow$$

$$(40.4) \qquad \omega_{2} = \frac{\sqrt{\beta_{1} + \beta_{2}}}{\sqrt{\mu}} \left( 1 - \frac{\alpha a^{2}}{32} k^{2} \right)$$

$$\omega = C k \qquad k \qquad \omega_{1}(k) \quad (39.4)$$

$$\omega_{ac} \qquad \omega_{1} \qquad k \qquad \omega_{2}(k) \qquad (40.4)$$

,

$$\omega_{op}$$
  $\omega_2$ 

$$: k = \pm \frac{\pi}{a}$$

$$\omega_{ac} \left(\pm \frac{\pi}{a}\right) = \omega_{ac}^{\text{max}} = \frac{\beta_1 + \beta_2}{2\mu} \left(1 - \sqrt{1 - \alpha}\right)$$
(41.4)

(42.4) 
$$\omega_{op} \left( \pm \frac{\pi}{a} \right) = \omega_{op}^{\min} = \sqrt{\frac{\beta_1 + \beta_2}{2\mu}} \left( 1 + \sqrt{1 - \alpha} \right)$$
$$\left( \beta_1 = \beta_2 \quad m = M : \right) \alpha = 1 \qquad \omega_{ac}^{\max} = \omega_{op}^{\min}$$

$$\omega_{ac}^{\text{max}} = \omega_{op}^{\text{min}} = 2\sqrt{\frac{\beta}{m}}$$

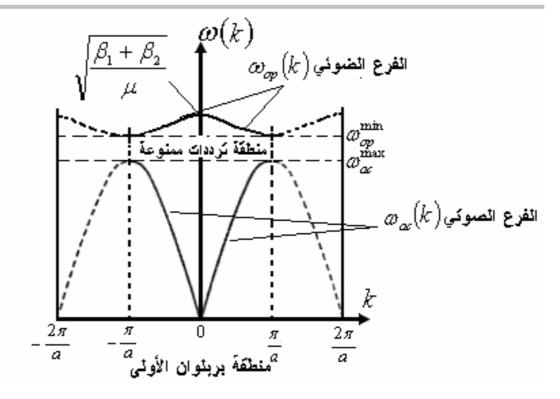
$$.\,\omega_{ac}\neq\omega_{op}\qquad \left(\,\beta_1\neq\beta_2\qquad m\neq M\,:\quad\,\right)\alpha\neq 1$$

•

$$(43.4) \omega_{ac}(k=0)=0$$

(44.4) 
$$\omega_{op}(k=0) = \sqrt{\frac{\beta_1 + \beta_2}{\mu}}$$

.



الشكل (9.4):

 $\omega_{op}^{\min}$  ,  $\omega_{ac}^{\max}$ 

• طبيعة المتزاز الدرات في الفرعين الصوتي و البصري

(45.4) 
$$\omega_{ac}(k=0) = 0$$

$$\omega_{op}(k=0) = \sqrt{\frac{\beta_1 + \beta_2}{\mu}}$$

$$\omega_{op}(k=0) = \sqrt{\frac{33.4}{45.4}}$$

$$\omega_{op}(k=0) = \sqrt{\frac{33.4}{45.4}}$$

(47.4) 
$$\frac{u_n}{v_n} = \frac{u}{v} = \frac{\beta_1 + \beta_2 \exp(ika)}{\beta_1 + \beta_2 - M\omega_{ac}^2(k=0)} = \frac{\beta_1 + \beta_2}{\beta_1 + \beta_2} = 1$$

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$$\frac{u_n}{v_n} = \frac{u}{v} = \frac{\beta_1 + \beta_2 \exp(ika)}{\beta_1 + \beta_2 - M\omega_{op}^2(k=0)} = \frac{\beta_1 + \beta_2}{\beta_1 + \beta_2 - M\sqrt{\frac{\beta_1 + \beta_2}{\mu}}} = -\frac{M}{m}$$

*M m* . (10.4)

 $(10.4) Mu_n + mu_n = 0$ 

الشكل (10.4):

$$.\left(k=\pm\frac{\pi}{a}\right)$$

(49.4) 
$$\omega_{ac} \left( \pm \frac{\pi}{a} \right) = \omega_{ac}^{\text{max}} = \frac{\beta_1 + \beta_2}{2\mu} \left( 1 - \sqrt{1 - \alpha} \right)$$

(50.4) 
$$\omega_{op}\left(\pm\frac{\pi}{a}\right) = \omega_{op}^{\min} = \sqrt{\frac{\beta_1 + \beta_2}{2\mu}}\left(1 + \sqrt{1-\alpha}\right)$$

(51.4) 
$$\frac{u_n}{v_n} = \frac{u}{v} = \frac{\beta_1 + \beta_2 \exp(ika)}{\beta_1 + \beta_2 - M\omega_{ac}^2(k = \pm \pi/a)} = \frac{\frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}}{1 - \frac{M + m}{2m}(1 - \sqrt{1 - \alpha})}$$

$$\vdots \qquad (50.4) \qquad (33.4) \quad (32.4) \quad (31.4) \quad (30.4)$$

(52.4) 
$$\frac{u_n}{v_n} = \frac{u}{v} = \frac{\beta_1 + \beta_2 \exp(ika)}{\beta_1 + \beta_2 - M\omega_{op}^2(k = \pm \pi/a)} = \frac{\frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}}{1 - \frac{M + m}{2m}(1 + \sqrt{1 - \alpha})}$$

 $\therefore m \neq M \qquad \beta_1 = \beta_2 \qquad \qquad .1$ 

$$: \quad (51.4) \qquad \quad \alpha$$

(53.4) 
$$\frac{u_n}{v_n} = \frac{\frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}}{1 - \frac{M + m}{2m} \left( 1 - \frac{|M - m|}{M + m} \right)}$$

$$v_n \neq 0 \quad u_n = 0 : \frac{u_n}{v_n} = \frac{0}{(m - M)/m} = 0 \qquad m > M$$

. m M

$$\alpha$$
: (52.4)

(54.4) 
$$\frac{u_n}{v_n} = \frac{\frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}}{1 - \frac{M + m}{2m} \left(1 + \frac{|M - m|}{M + m}\right)}$$

$$v_n \neq 0 \quad u_n = 0 \quad \frac{u_n}{v_n} = \frac{0}{(m - M)/m} = 0 \qquad M > m$$

.

 $: \beta_1 > \beta_2 \qquad m = M \qquad \qquad . \mathbf{2}$ 

(55.4)  $\frac{u_n}{v_n} = \frac{\frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}}{1 - \left(1 - \frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}\right)} = 1$ 

M

(56.4)  $\frac{u_n}{v_n} = \frac{\frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}}{1 - \left(1 + \frac{\beta_1 - \beta_2}{\beta_1 + \beta_2}\right)} = -1$ 

m M

4-5 الأنماط الطبيعية لشبكة براضي ثلاثية الأبعاد

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N

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.  $\vec{a}_3, \vec{a}_2, \vec{a}_1$ 

.

(57.4) 
$$\vec{u}(\vec{r},t) = \vec{\varepsilon} \exp(i(\vec{k}.\vec{r} - \omega t))$$

$$: \vec{\varepsilon} \cdot t \qquad \vec{r} \qquad ( ) \qquad : \vec{u}(\vec{r},t)$$

$$: \vec{k}$$

 $\omega = f(k)$ 

:

(58.4) 
$$\vec{u}(\vec{r},t) = \vec{u}(\vec{r} + N_i \vec{a}_i, t)$$
  
 $N_i(i=1,2,3)$   $\vdots \vec{a}_i(i=1,2,3)$ 

 $(23) N = N_1 N_2 N_3$ 

(59.4) 
$$\exp(iN_i\vec{k}.\vec{a}_i) = 1$$
  $i = 1,2,3$ 

:  $ec{k}$ 

(60.4) 
$$\vec{k} = \sum_{i=1}^{3} \frac{n_i}{N_i} \vec{A}_i \qquad i = 1,2,3$$

$$A_i = \frac{2\pi}{a_i} (i = 1,2,3) \qquad n_i (i = 1,2,3)$$

.

(61.4) 
$$\vec{a}_i \cdot \vec{A}_j = 2\pi \delta_{ij}$$
  $i, j = 1,2,3$ 

:  $ec{G}$ 

) 
$$\vec{k} = \exp(i\vec{k}.\vec{R}) = 1$$
 
$$\vec{k}$$
 .(

 $ec{k}$  ,  $ec{k}' = ec{k} + ec{G}$ 

 $\vec{k} \tag{60.4}$ 

(62.4) 
$$\vec{k}_{A_i} = \frac{n_i}{N_i} \vec{A}_i$$

 $\vec{k}$ 

 $\vec{k}_{\scriptscriptstyle A_i}$  $\vec{k}$ 

(63.4) 
$$\Delta \vec{k}_{A_1} \cdot \left(\Delta \vec{k}_{A_2} \times \Delta \vec{k}_{A_3}\right) = \frac{\vec{A}_1}{N_1} \cdot \left(\frac{\vec{A}_2}{N_2} \times \frac{\vec{A}_3}{N_3}\right) = \frac{V_e^*}{N}$$

 $V_e^*$ 

 $\vec{k}$ 

 $\frac{V_e^*}{\left(\frac{V_e^*}{N}\right)} = N$ (64.4)

 $\vec{\varepsilon}_p(\vec{k})(p=1,2,3)$ 

N

 $\omega_p(\vec{k})(p=1,2,3)$ 

 $\cdot \left(\omega_p\left(\vec{k}\to 0\right)\right)\to 0$ 

 $\omega_p(\vec{k})(p=1,2,3,....3\varsigma)$ N

 $(\omega_p(\vec{k} \to 0)) \to \omega_{\text{max}} \neq 0$  :  $3(\varsigma - 1)$ 

) 
$$. \vec{k} \qquad (11.4)$$

 $\omega(\vec{k})$  فروع ضوئية فروع صوتية  $\vec{k}$  اتجاه بٽوري غير تناضري

:(11.4)

• كثافة الأنماط لشبكة برافي ثلاثية الأبعاد أحادية الدرة(في تقريب ديباي)

$$\vec{k}$$
 
$$\vec{k}$$
 
$$\vec{k}$$
 
$$|(V_e^*/N)|$$
 
$$k + dk \quad k$$
 
$$\vec{k}$$
 
$$\{1/(V_e^*/N) = (N/V_e^*)\}$$
 
$$: dk \quad \vec{k}$$

(65.4) 
$$g(k)dk = \frac{N}{V_e^*} 4\pi k^2 dk$$

) 
$$N$$
 :  $V_e V_e^* = \frac{(2\pi)^3}{V_e}$  :

:  $V=NV_e$  (

$$(66.4) g(k)dk = \frac{V}{2\pi^2}k^2dk$$

k  $: \omega + d\omega \quad \omega$ 

 $d\omega$ 

(67.4) 
$$D(\omega)d\omega = 3g(k)dk$$

:  $D(\omega)$ 

(68.4) 
$$D(\omega)d\omega = 3\frac{V}{2\pi^2}k^2dk$$

:

(69.4) 
$$\omega = v_g k = v_p k = v_S k$$

 $V_g, V_p, V_S$ :

(70.4) 
$$D(\omega)d\omega = 3\frac{V}{2\pi^2} \frac{\omega^2}{v_S^3} d\omega$$

 $(\omega_{\text{max}} = \omega_D)$   $(\omega_{\text{min}} = 0)$ 

 $k_{\scriptscriptstyle D}$   $ec{k}$  k  $\omega_{\scriptscriptstyle D}$ 

)

: .(

(71.4) 
$$3N = \int_{0}^{\omega_{D}} D(\omega) d\omega$$

$$3N = \int_{0}^{\omega_{D}} 3 \frac{V}{2\pi^{2}} \frac{\omega^{2}}{V_{S}^{3}} d\omega$$

А

(72.4) 
$$\omega_D = \sqrt[3]{\left(\frac{6N\pi^2}{V}\right)} \mathbf{v}_S = \sqrt[3]{6\pi^2 n_a} \mathbf{v}_S$$

(73.4) 
$$k_D = \sqrt[3]{\left(\frac{6N\pi^2}{V}\right)} = \sqrt[3]{6\pi^2 n_a}$$

.  $k_D$   $n_a$ 

$$(74.4) D_D(\omega) = \frac{9N}{\omega_D^3} \omega^2$$

#### 6-4 تكميم الهتزازات الشبكة البلورية

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(75.4) 
$$E_{n_{k,p}} = \left(n_{\vec{k},p} + \frac{1}{2}\right)\hbar\omega_p(\vec{k})$$

$$p$$
 ( )  $ec{k}$  ( الموافق له )  $:\omega_p(ec{k})$ 

```
: \varsigma \qquad p = 1, 2, 3 \dots 3\varsigma
n_{\vec{k},p}
                                                                                                                                                                                      n_{\vec{k},p}
                                                (
                                                                                                                         3N\varsigma
                                                                                                                                                                                         N
                                                                                                                                                                   : \frac{1}{2}\hbar\omega_p(\vec{k})
                                          (n_{\vec{k},p}=0)
                                                                                                                                                                           (12.4)
                                                      U_{tot} = \sum_{\vec{k},p} E_{n_{k,p}} = \sum_{\vec{k},p} \left( n_{\vec{k},p} + \frac{1}{2} \right) \hbar \omega_p(\vec{k})
(76.4)
                                                                                    n_{\vec{k},p} \hbar \omega_p(\vec{k})
                                                                                                                                              (12.4)
                                                                                                                                                                           (\vec{k}, p)
```

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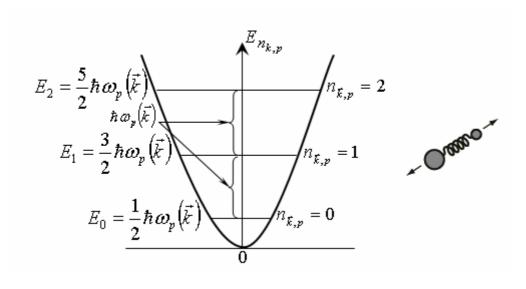
$$(77.4) \vec{K}' = \vec{K} + \vec{G}$$

 $ec{K}'$   $ec{K}$   $ec{G}$ 

 $\left(-\hbar\vec{G}\right)$ 

(absorption) (creation)

 $(78.4) \vec{K}' = \vec{K} + \vec{G} \pm \vec{k}_p$ 



:(12.4)

## 7-4 الخصائص الحرارية

#### 4-7-1 السعة الحرارية

:

(79.4) 
$$\Delta Q = C_s m \Delta T = C \Delta T$$

 $(C_s) (C_s m = C)$ 

 $C_p$   $C_v$  . (

:

(80.4) 
$$\Delta Q = \Delta U - W \Rightarrow \Delta Q = \Delta U \quad (W = 0)$$

$$C = \frac{\Delta Q}{\Delta T} = \frac{\Delta U}{\Delta T}$$
(13.4)

:

(

 $R 3R = 25 J / mole \overset{\circ}{k} = 6 cal / mol. \overset{\circ}{K}$ 

 $20\overset{\circ}{k}$ 

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:

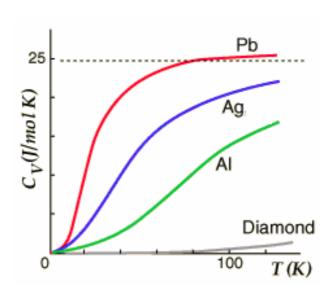
$$C = aT^3 + \gamma T$$

$$C = aT^3$$

$$C = aT^2$$

سنحاول

.



:(13.4)

أ- السعة الحرارية وفق النموذج الكلاسيكي

\_

$$(K_BT/2)$$
 (N)  $(K_BT)$ 

:

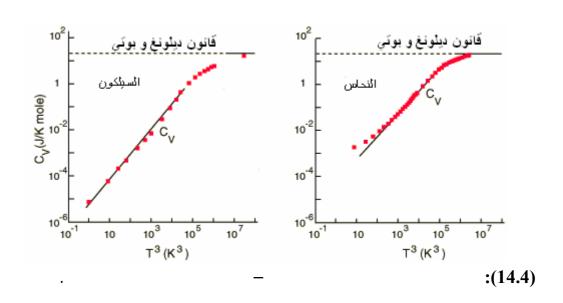
(81.4) 
$$\langle U_{tot} \rangle = 3NK_B T$$

: 
$$N_A = 6.022 \ 10^{23}$$

(82.4) 
$$\langle U_{tot} \rangle = 3N_A KT = 3RT$$

: 
$$R = N_A K_B \approx 2 \, cal / mol. \overset{\circ}{K}$$

(83.4) 
$$C = \frac{d\langle U_{tot} \rangle}{dT} = 3R \approx 6cal / mol. K = 25 J / mol. K$$
((14.4) ) (Dulong-Petit) –



## ب- نموذج أينشتاين السعة الحرارية

 $\omega_E$ 

:

(84.4) 
$$E_n = n\hbar\omega$$
  $n = 0,1,2,3,...$  ((12.4)

•

(85.4) 
$$E_n = \left(n + \frac{1}{2}\right)\hbar\omega \qquad n = 0,1,2,3...$$

n=0

n=0

 $\langle E \rangle$ 

N

(86.4) 
$$N = \sum_{n} N(E_{n}) \\ E = \sum_{n} N(E_{n})E_{n} \Rightarrow \langle E \rangle = \frac{E}{N} = \frac{\sum_{n} N(E_{n})E_{n}}{\sum_{n} N(E_{n})}$$

(86.4)

(87.4) 
$$\langle E \rangle = \frac{\int_{0}^{\infty} N(E) E dE}{\int_{0}^{\infty} N(E) dE}$$

$$E_n$$
  $\left(e^{\frac{-E}{K_BT}}\right)$ 

:(86.4)

(88.4) 
$$\langle E \rangle = \frac{\sum_{n=0}^{\infty} n\hbar \omega e^{\frac{-n\hbar\omega}{K_B T}}}{\sum_{n=0}^{\infty} e^{\frac{-n\hbar\omega}{K_B T}}}$$

$$\langle E \rangle = \frac{0 + \hbar \omega e^{\frac{-\hbar \omega}{K_B T}} + 2\hbar \omega e^{\frac{-2\hbar \omega}{K_B T}} + \dots }{1 + e^{\frac{-\hbar \omega}{K_B T}} + e^{\frac{-2\hbar \omega}{K_B T}} + \dots}$$

 $\therefore \qquad x = \frac{-\hbar\omega}{K_B T}$ 

(89.4) 
$$\langle E \rangle = \frac{\hbar \omega e^{x} (1 + 2e^{x} + 3e^{2x} + \dots)}{1 + e^{x} + e^{2x} + \dots}$$

$$\left(\frac{1}{\left(1-e^{x}\right)^{2}}\right)$$

$$(89.4) \qquad \qquad \left(\frac{1}{1-e^x}\right)$$

(90.4) 
$$\langle E \rangle = \frac{\hbar \omega e^x}{1 - e^x} = \frac{\hbar \omega}{e^{-x} - 1} = \frac{\hbar \omega}{e^{\frac{\hbar \omega}{K_B T}} - 1}$$

 $: 3N_A$ 

(91.4) 
$$\langle U_{tot} \rangle = 3N \frac{\hbar \omega}{e^{\frac{\hbar \omega}{K_B T}} - 1} = 3N_A \frac{\hbar \omega}{e^{\frac{\theta_E}{T}} - 1}$$

 $\theta_E = \frac{\hbar \omega}{K_B}$ 

•

(92.4) 
$$C_{v} = \frac{d \langle U_{tot} \rangle}{dT} = \frac{3N_{A}K_{B} \left(\frac{\hbar \omega}{K_{B}T}\right)^{2} e^{\frac{\hbar \omega}{K_{B}T}}}{\left(e^{\frac{\hbar \omega}{K_{B}T}} - 1\right)^{2}}$$

$$\vdots \qquad (92.4)$$

1) الدراسة عند المجالات الحرارية العالية

 $(K_B T >> \hbar \omega)$ 

(93.4) 
$$e^{\frac{\hbar\omega}{K_BT}} - 1 = 1 + \frac{\hbar\omega}{K_BT} + \left(\frac{\hbar\omega}{K_BT}\right)^2 + \dots - 1 \approx \frac{\hbar\omega}{K_BT}$$

: (92.4) (93.4)

(94.4) 
$$C_{v} = 3N_{A}K_{B} \left( 1 + \frac{\hbar\omega}{K_{B}T} \right) = 3N_{A}K_{B} + \frac{\hbar\omega}{T} \approx 3N_{A}K_{B} = 3R$$

$$(94.4)$$

2) الدراسة عند المحالات الحرارية المنخفضة

$$(92.4) (K_BT << \hbar\omega)$$

$$C_{v} = \frac{d \left\langle E \right\rangle_{tot}}{dT} = \frac{3 N_{A} K_{B} \left(\frac{\hbar \omega}{K_{B} T}\right)^{2} e^{\frac{\hbar \omega}{K_{B} T}}}{\left(e^{\frac{\hbar \omega}{K_{B} T}}\right)^{2}} = 3 N_{A} K_{B} \left(\frac{\hbar \omega}{K_{B} T}\right)^{2} e^{\frac{-\hbar \omega}{K_{B} T}}$$

(95.4) 
$$C_{v} = 3R \left(\frac{\hbar \omega}{K_{B}T}\right)^{2} e^{\frac{-\hbar \omega}{K_{B}T}} = 3R \left(\frac{\theta_{E}}{T}\right)^{2} e^{\frac{-\theta_{E}}{T}}$$

$$\text{(T=0)} \tag{95.4}$$

.

ج- نموذج ديباي السعة الحرارية

$$(\omega_{\min} \le \omega \le \omega_{\max})$$

$$(\omega_{\min} = 0)$$

$$(\omega_{\min} = \omega_D)$$

 $\langle U_{tot} \rangle = \int_{0}^{E_{\text{max}}} \langle E \rangle dN(E) = \int_{0}^{\omega_{\text{max}}} \frac{\hbar \omega}{e^{\frac{\hbar \omega}{K_B T}} - 1} D(\omega) d\omega$ 

(95.4) 
$$\langle U_{tot} \rangle = \int_{0}^{\omega_{D}} \frac{\hbar \omega}{e^{\frac{\hbar \omega}{K_{B}T}} - 1} D_{D}(\omega) d\omega$$

$$: ((74.4) )$$

(96.4) 
$$D_{D}(\omega) = \frac{9N}{\omega_{D}^{3}} \omega^{2}$$

$$: (95.4) \qquad (96.4)$$

(97.4) 
$$\langle U_{tot} \rangle = \frac{9N}{\omega_D^3} \int_0^{\omega_D} \frac{\hbar \omega^3}{e^{\frac{\hbar \omega}{K_B T}} - 1} . d\omega$$

$$x = \frac{\hbar \omega}{K_B T}$$

$$x = \frac{\hbar \omega}{K_B T} \Rightarrow \omega = \frac{K_B T}{\hbar} x \Rightarrow d\omega = \frac{K_B T}{\hbar} dx$$

(98.4) 
$$\omega^3 d\omega = \frac{K_B^3 T^3 x^3}{\hbar^3} \cdot \frac{K_B T}{\hbar} dx \Rightarrow \frac{K_B^4 T^4 x^3}{\hbar^4} dx$$

$$(99.4) x = 0 \Rightarrow \omega = 0$$

(100.4) 
$$\omega_{\text{max}} = \omega_D = \frac{K_B T}{\hbar} x_{\text{max}} \Rightarrow x_{\text{max}} = \frac{\hbar \omega_D}{K_B T} = \frac{\theta_D}{T}$$

.  $\theta_{\scriptscriptstyle D} = \frac{\hbar \omega_{\scriptscriptstyle D}}{K_{\scriptscriptstyle B}}$ 

: (97.4) (100.4) (99.4) (98.4)

(101.4) 
$$\langle U_{tot} \rangle = \frac{9NK_B T^4}{\theta_D^3} \int_0^{x_{max}} \frac{x^3}{e^x - 1} dx$$

(102.4) 
$$C_{v} = 9NK_{B} \left(\frac{T}{\theta_{D}}\right)^{3} \int_{0}^{\frac{\theta_{D}}{T}} \frac{x^{4}e^{x}}{\left(e^{x}-1\right)^{2}} dx$$

(102.4) (101.4)

أ- الدراسة عند الدرجات الحرارية العالية

$$(103.4) \frac{x^3}{e^x - 1} = \frac{x^3}{1 + x + x^2 + \dots} \approx \frac{x^3}{x} = x^2$$

$$\langle U_{tot} \rangle = \frac{9NK_B T^4}{\theta_D^3} \int_0^{x_{\text{max}}} \frac{x^3}{e^x - 1} dx = \frac{9NK_B T^4}{\theta_D^3} \int_0^{x_{\text{max}}} x^2 dx$$

$$\langle U_{tot} \rangle = \frac{9NK_B T^4}{\theta_D^3} \cdot \frac{x_{\text{max}}^3}{3} = \frac{9NK_B T^4}{\theta_D^3} \cdot \frac{\theta_D^3}{3T^3} = 3NK_B T$$

$$(104.4)$$

$$C_v = \frac{d\langle U \rangle}{dT} = 3NK_B$$

$$: \qquad N = N_A$$

$$(105.4) C_{v} = 3N_{A}K_{B} = 3R$$

. – (105.4)

ب- الدراسة عند الدرجات الحرارية المنخفضة

$$(0 \mapsto (x_{\text{max}} \to \infty)) \qquad K_B T << \hbar \omega$$

.

(106.4) 
$$\int_{0}^{\infty} \frac{x^{3}}{e^{x} - 1} dx = \frac{\pi^{4}}{15}$$

: (101.4)

$$\langle U_{tot} \rangle = \frac{9NK_B T^4}{\theta_D^3} \int_0^{\infty} \frac{x^3}{e^x - 1} dx = \frac{9NK_B T^4}{\theta_D^3} \cdot \frac{\pi^4}{15} = \frac{3\pi^4 NK_B T^4}{5\theta_D^3}$$

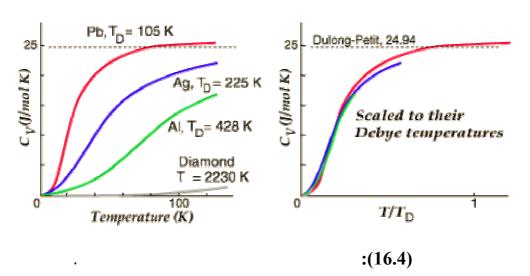
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(107.4) 
$$C_{v} = \frac{d\langle U \rangle}{dT} = \frac{12\pi^{4}N_{A}K_{B}T^{3}}{5\theta_{D}^{3}} = \frac{12}{5}\pi^{4}R\left(\frac{T}{\theta_{D}}\right)^{3}$$
(107.4) 
$$(15.4) \qquad (107.4)$$
(107.4)

Fit of silver specific heat data to the Debye curve with  $T_D = 215 \text{ K}$ .

T/ $T_D$  I

( ) :(15.4)



: (1.4)

$ heta_{\scriptscriptstyle D}$ درجةحرارة ديباي	العنصر	$ heta_{\scriptscriptstyle D}\!\!\left(\stackrel{o}{K} ight)$ درجةحرارة ديباي	العنصر
230	Ca	428	Al
630	Cr	110	Pb
450	Mn	158	Na
467	Fe	370	Li
343	Cu	1160	Be
310	Zn	164	Au
370	Ge	640	Si
732	LiF	470	SiO <sub>2</sub>
510	CaF <sub>2</sub>	321	NaCl

:(1.4)

## 2-7-4 الاهتزازات اللاتوافقية

(108.4) 
$$F(x) = -\beta x + \gamma x^2 - \alpha x^3$$

: x

$$(109.4) F(x) = -\beta x$$

 $\boldsymbol{X}$ 

:

(110.4) 
$$U(x) = -f x^{2} - g x^{3} + h x^{4}$$

$$x^{3} \qquad f, g, h:$$

... ( )

## 3-7-4 التمدد الحراري

. عد

T X

: x

(111.4) 
$$\langle x \rangle = \frac{\int\limits_{-\infty}^{+\infty} x \exp\left(-\frac{U(x)}{K_B T}\right) dx}{\int\limits_{-\infty}^{+\infty} \exp\left(-\frac{U(x)}{K_B T}\right) dx}$$

(110.4)

: (111.4)

$$\int_{-\infty}^{+\infty} x \exp\left(-\frac{U(x)}{K_B T}\right) dx = \int_{-\infty}^{+\infty} x \exp\left(-\frac{f x^2}{K_B T}\right) \cdot \int_{-\infty}^{+\infty} \exp\left(-\frac{g x^3 + h x^4}{K_B T}\right) dx$$

$$\cong \int_{-\infty}^{+\infty} x \exp\left(-\frac{f x^2}{K_B T}\right) \cdot \left(1 + \frac{g}{K_B T} x^3 + \frac{h}{K_B T} x^4 + \dots\right) dx$$

$$= \int_{-\infty}^{+\infty} \exp\left(-\frac{f x^2}{K_B T}\right) \cdot \left(x + \frac{g}{K_B T} x^4 + \frac{h}{K_B T} x^5 + \dots\right) dx$$

$$= \int_{-\infty}^{+\infty} x \exp\left(-\frac{f x^2}{K_B T}\right) \cdot dx + \frac{g}{K_B T} \int_{-\infty}^{+\infty} x^4 \exp\left(-\frac{f x^2}{K_B T}\right) dx + \frac{h}{K_B T} \int_{-\infty}^{+\infty} x^5 \exp\left(-\frac{f x^2}{K_B T}\right) dx + \dots$$

$$x^5 \quad x$$

:

(112.4) 
$$\int_{-\infty}^{+\infty} x \exp\left(-\frac{U(x)}{K_B T}\right) dx \cong \frac{g}{K_B T} \int_{-\infty}^{+\infty} x^4 \exp\left(-\frac{f x^2}{K_B T}\right) = dx \frac{3g\sqrt{\pi}}{4K_B T} \left(\frac{K_B T}{f}\right)^{\frac{5}{2}}$$

.

(113.4) 
$$\int_{-\infty}^{+\infty} \exp\left(-\frac{U(x)}{K_B T}\right) dx \cong \int_{-\infty}^{+\infty} \exp\left(-\frac{f x^2}{K_B T}\right) dx = \left(\frac{\pi K_B T}{f}\right)^{\frac{1}{2}}$$

.

$$\langle x \rangle = \frac{3K_B T}{4f^2} g$$

 $\langle x 
angle$ 

(115.4) 
$$\alpha = \frac{\langle x \rangle}{aT} = \frac{3K_B T}{4a f^2} g$$

g = 0 .

## 4-7-4 التوصيل الحراري في العوازل

Q

dX dT

(dT/dX)

(116.4)

$$Q = K \left( \frac{dT}{dX} \right)$$

. K

1

.

(117.4) 
$$K = \frac{1}{3}C\langle v \rangle \lambda$$

## 1. قانون حفظ الطاقة

(119.4) 
$$\hbar\omega_1 + \hbar\omega_2 = \hbar\omega_3$$
$$\omega_1 + \omega_2 = \omega_3$$

### 2 قانون حفظ كمية الحركة

 $\vec{k}_2, \vec{k}_1$ :

$$N$$
 :قولية العادية  $ar{k}_3$  : العملية العادية العادية العادية  $N$  :  $N$  :

- عملية الانقلاب: U (UmKlapp)  $\left(\vec{k}_3' = \vec{k}_1 + \vec{k}_2\right) \vec{k}_3'$  $K_p$ 

 $\lambda_3'$ 

 $. \qquad \vec{k}_2, \vec{k}_1$ 

 $k_3 = k_2 - \frac{\pi}{2}$  :  $\vec{k}_3$ 

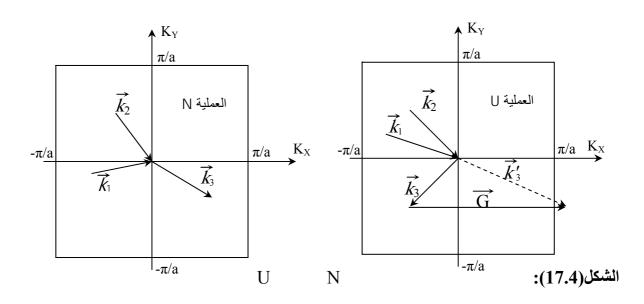
(Peierls)

erls) .  $\vec{G}$  (120.4)

 $(121.4) \vec{k}_1 + \vec{k}_2 = \vec{k}_3 + \vec{G}$ 

.  $ec{G}$ 

.U  $\vec{G} \neq \vec{0}$  N  $\vec{G} = \vec{0}$ 



ب- التشتت بالعيوب البلورية

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1 – العيوب النقطية

4

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2 – العيوب الخطية

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3 - أو كليهما.

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ت- التشتت عند حواف العينة

U

D

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(122.4) K = C V D  $(T << \theta_D ) T^3$ 

 $_{\prime}(T>\theta_{D})$ 

r

$$(K_B\theta_D/2)$$

 $\exp(\theta_D/2T)$ 

(123.4) 
$$\lambda \propto \exp(\theta_D/2T)$$
$$K_P \propto \exp(\theta_D/2T)$$

(2.4)  $T = 20 \overset{\circ}{K}, T = 273 \overset{\circ}{K}$ 

T =	20 K	$T = 273 \overset{\circ}{K}$		
λ[Å]	$K \Big[W \Big/m. \overset{\circ}{K}\Big]$	λ[Å]	$K \left[ W / m. \mathring{K} \right]$	
0.0075	760	97	14	SiO <sub>2</sub>
0.001	85	72	11	CaF <sub>2</sub>
0.00023	45	67	6.4	NaCl
0.041	4200	430	150	Si
0.0045	1300	330	70	Ge

الجدول(2.4):

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