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Transfert de chaleur (3L)

Module : Année : 21/20 Spécialité : Groupe : Durée : min
Nom et prénom : الاسم واللقب: Matricule:

Basic Heat-Transfer Relations

Fourier's law of heat conduction:

$$q_x = -kA \frac{\partial T}{\partial x}$$

Characteristic thermal resistance for conduction = $\Delta x/kA$

Characteristic thermal resistance for convection = $1/hA$

Overall heat transfer = $\Delta T_{\text{overall}} / \Sigma R_{\text{thermal}}$

Convection heat transfer from a surface:

$$q = hA(T_{\text{surface}} - T_{\text{free stream}}) \quad \text{for exterior flows}$$

$$q = hA(T_{\text{surface}} - T_{\text{fluid bulk}}) \quad \text{for flow in channels}$$

Forced convection: $Nu = f(Re, Pr)$

Free convection: $Nu = f(Gr, Pr)$

$$Re = \frac{\rho u x}{\mu} \quad Gr = \frac{\rho^2 g \beta \Delta T x^3}{\mu^2} \quad Pr = \frac{c_p \mu}{k}$$

x = characteristic dimension

Blackbody emissive power, $\frac{\text{energy emitted by blackbody}}{\text{area} \cdot \text{time}} = \sigma T^4$

Radiosity = $\frac{\text{energy leaving surface}}{\text{area} \cdot \text{time}}$

Irradiation = $\frac{\text{energy incident on surface}}{\text{area} \cdot \text{time}}$

Radiation shape factor F_{mn} = fraction of energy leaving surface m and arriving at surface n

Reciprocity relation: $A_m F_{mn} = A_n F_{nm}$

Radiation heat transfer from surface with area A_1 , emissivity ϵ_1 , and temperature T_1 (K) to large enclosure at temperature T_2 (K):

$$q = \sigma A_1 \epsilon_1 (T_1^4 - T_2^4)$$

LMTD method for heat exchangers :

$$q = UAF \Delta T_m$$

where F = factor for specific heat exchanger; ΔT_m = LMTD for counterflow double-pipe heat exchanger with same inlet and exit temperatures

Effectiveness-NTU method for heat exchangers :

$$\epsilon = \frac{\text{Temperature difference for fluid with minimum value of } mc}{\text{Largest temperature difference in heat exchanger}}$$

$$NTU = \frac{UA}{C_{\min}} \quad \epsilon = f(NTU, C_{\min}/C_{\max})$$

See List of Symbols on next page for definitions of terms.



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Transfert thermique et Echangeurs de chaleur & Phénomène de Transfert II

Module : **UEM1.1** Année : 21/20 Spécialité :Groupe : Durée : 60 min

Nom et prénom :: الاسم واللقب: Matricule:

Convection Heat Transfer

$$Re = \frac{\rho V L_c}{\mu} = \frac{V L_c}{\nu} \quad [\text{Reynolds Number}] \quad ; \quad \overline{Nu} = \frac{\bar{h} L_c}{k_f} \quad [\text{Average Nusselt Number}]$$

where ρ is the density, V is the velocity, L_c is the characteristic length, μ is the dynamic viscosity, ν is the kinematic viscosity, \dot{m} is the mass flow rate, \bar{h} is the average convection coefficient, and k_f is the fluid thermal conductivity.

Internal Flow

$$Re = \frac{4 \dot{m}}{\pi D \mu} \quad [\text{For Internal Flow in a Pipe of Diameter } D]$$

For Constant Heat Flux [$q_s'' = \text{constant}$]: $q_{conv} = q_s''(P \cdot L)$; where P = Perimeter, L = Length

$$T_m(x) = T_{m,i} + \frac{q_s'' \cdot P}{\dot{m} \cdot c_p} x$$

For Constant Surface Temperature [$T_s = \text{constant}$]:

If there is only convection between the surface temperature, T_s , and the mean fluid temperature, T_m , use

$$\frac{T_s - T_m(x)}{T_s - T_{m,i}} = \exp\left(-\frac{P \cdot x}{\dot{m} \cdot c_p} \bar{h}\right)$$

If there are multiple resistances between the outermost temperature, T_∞ , and the mean fluid temperature, T_m , use

$$\frac{T_\infty - T_m(x)}{T_\infty - T_{m,i}} = \exp\left(-\frac{P \cdot x}{\dot{m} \cdot c_p} U\right) = \exp\left(-\frac{1}{\dot{m} \cdot c_p \cdot R_t}\right)$$

Total heat transfer rate over the entire tube length:

$$q_t = \dot{m} \cdot c_p \cdot (T_{m,o} - T_{m,i}) = \bar{h} \cdot A_s \cdot \Delta T_{lm} \text{ or } U \cdot A_s \cdot \Delta T_{lm} \quad ; \quad T_s = \text{constant}$$

Log mean temperature difference: $\Delta T_{lm} = \frac{\Delta T_o - \Delta T_i}{\ln\left(\frac{\Delta T_o}{\Delta T_i}\right)}$; $\Delta T_o = T_s - T_{m,o}$; $\Delta T_i = T_s - T_{m,i}$



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Résumé des corrélations de transfert de chaleur par convection pour le flux externe

Correlation	Geometry	Conditions ^c
$\delta = 5x Re_x^{-1/2}$	Flat plate	Laminar, T_f
$C_{f,x} = 0.664 Re_x^{-1/2}$	Flat plate	Laminar, local, T_f
$Nu_x = 0.332 Re_x^{1/2} Pr^{1/3}$	Flat plate	Laminar, local, T_f , $Pr \geq 0.6$
$\delta_t = \delta Pr^{-1/3}$	Flat plate	Laminar, T_f
$\bar{C}_{f,x} = 1.328 Re_x^{-1/2}$	Flat plate	Laminar, average, T_f
$\bar{Nu}_x = 0.664 Re_x^{1/2} Pr^{1/3}$	Flat plate	Laminar, average, T_f , $Pr \geq 0.6$
$Nu_x = 0.564 Pe_x^{1/2}$	Flat plate	Laminar, local, T_f , $Pr \leq 0.05$, $Pe_x \geq 100$
$C_{f,x} = 0.0592 Re_x^{-1/5}$	Flat plate	Turbulent, local, T_f , $Re_x \leq 10^8$
$\delta = 0.37x Re_x^{-1/5}$	Flat plate	Turbulent, T_f , $Re_x \leq 10^8$
$Nu_x = 0.0296 Re_x^{4/5} Pr^{1/3}$	Flat plate	Turbulent, local, T_f , $Re_x \leq 10^8$, $0.6 \leq Pr \leq 60$
$\bar{C}_{f,L} = 0.074 Re_L^{-1/5} - 1742 Re_L^{-1}$	Flat plate	Mixed, average, T_f , $Re_{x,c} = 5 \times 10^5$, $Re_L \leq 10^8$
$\bar{Nu}_L = (0.037 Re_L^{4/5} - 871) Pr^{1/3}$	Flat plate	Mixed, average, T_f , $Re_{x,c} = 5 \times 10^5$, $Re_L \leq 10^8$, $0.6 \leq Pr \leq 60$
$\bar{Nu}_D = C Re_D^m Pr^{1/3}$ (Table 7.2)	Cylinder	Average, T_f , $0.4 \leq Re_D \leq 4 \times 10^5$, $Pr \geq 0.7$
$\bar{Nu}_D = C Re_D^m Pr^n (Pr/Pr_s)^{1/4}$ (Table 7.4)	Cylinder	Average, T_∞ , $1 \leq Re_D \leq 10^6$, $0.7 \leq Pr \leq 500$
$\bar{Nu}_D = 0.3 + [0.62 Re_D^{1/2} Pr^{1/3} \times [1 + (0.4/Pr)^{2/3}]^{-1/4}] \times [1 + (Re_D/282,000)^{5/8}]^{4/5}$	Cylinder	Average, T_f , $Re_D Pr \geq 0.2$
$\bar{Nu}_D = 2 + (0.4 Re_D^{1/2} + 0.06 Re_D^{2/3}) Pr^{0.4} \times (\mu/\mu_s)^{1/4}$	Sphere	Average, T_∞ , $3.5 \leq Re_D \leq 7.6 \times 10^4$, $0.71 \leq Pr \leq 380$, $1.0 \leq (\mu/\mu_s) \leq 3.2$



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Nom et prénom ::الاسم واللقب: Matricule:.....

Résumé des corrélations de convection pour l'écoulement dans un tube circulaire

Correlation	Conditions
$f = 64/Re_D$	Laminar, fully developed
$Nu_D = 4.36$	Laminar, fully developed, uniform q_s''
$Nu_D = 3.66$	Laminar, fully developed, uniform T_s
$\bar{Nu}_D = 3.66 + \frac{0.0668 Gz_D}{1 + 0.04 Gz_D^{2/3}}$	Laminar, thermal entry (or combined entry with $Pr \geq 5$), uniform T_s , $Gz_D = (D/x) Re_D Pr$
$\bar{Nu}_D = \frac{3.66}{\tanh[2.264 Gz_D^{-1/3} + 1.7 Gz_D^{-2/3}]} + 0.0499 Gz_D \tanh(Gz_D^{-1})}$ $\tanh(2.432 Pr^{1/6} Gz_D^{-1/6})$	Laminar, combined entry, $Pr \geq 0.1$, uniform T_s , $Gz_D = (D/x) Re_D Pr$
$\frac{1}{\sqrt{f}} = -2.0 \log \left[\frac{e/D}{3.7} + \frac{2.51}{Re_D \sqrt{f}} \right]$	Turbulent, fully developed
$f = (0.790 \ln Re_D - 1.64)^{-2}$	Turbulent, fully developed, smooth walls, $3000 \leq Re_D \leq 5 \times 10^6$
$Nu_D = 0.023 Re_D^{4/5} Pr^n$	Turbulent, fully developed, $0.6 \leq Pr \leq 160$, $Re_D \geq 10,000$, $(L/D) \geq 10$, $n = 0.4$ for $T_s > T_m$ and $n = 0.3$ for $T_s < T_m$
$Nu_D = 0.027 Re_D^{4/5} Pr^{1/3} \left(\frac{\mu}{\mu_s} \right)^{0.14}$	Turbulent, fully developed, $0.7 \leq Pr \leq 16,700$, $Re_D \geq 10,000$, $L/D \geq 10$
$Nu_D = \frac{(f/8)(Re_D - 1000) Pr}{1 + 12.7(f/8)^{1/2}(Pr^{2/3} - 1)}$	Turbulent, fully developed, $0.5 \leq Pr \leq 2000$, $3000 \leq Re_D \leq 5 \times 10^6$, $(L/D) \geq 10$
$Nu_D = 4.82 + 0.0185(Re_D Pr)^{0.827}$	Liquid metals, turbulent, fully developed, uniform q_s'' , $3.6 \times 10^3 \leq Re_D \leq 9.05 \times 10^5$, $3 \times 10^{-3} \leq Pr \leq 5 \times 10^{-2}$, $10^2 \leq Re_D Pr \leq 10^4$
$Nu_D = 5.0 + 0.025(Re_D Pr)^{0.8}$	Liquid metals, turbulent, fully developed, uniform T_s , $Re_D Pr \geq 100$



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Transfert thermique et Echangeurs de chaleur

Module : Année : 21/22 Spécialité : Groupe : Durée : .. min
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Distributions de température et flux de chaleur pour les ailettes de section uniforme

Case	Tip Condition ($x = L$)	Temperature Distribution θ/θ_b	Fin Heat Transfer Rate q_f
A	Convection: $h\theta(L) = -kd\theta/dx _{x=L}$	$\frac{\cosh m(L-x) + (h/mk) \sinh m(L-x)}{\cosh mL + (h/mk) \sinh mL}$ (3.75)	$M \frac{\sinh mL + (h/mk) \cosh mL}{\cosh mL + (h/mk) \sinh mL}$ (3.77)
B	Adiabatic: $d\theta/dx _{x=L} = 0$	$\frac{\cosh m(L-x)}{\cosh mL}$ (3.80)	$M \tanh mL$ (3.81)
C	Prescribed temperature: $\theta(L) = \theta_L$	$\frac{(\theta_L/\theta_b) \sinh mx + \sinh m(L-x)}{\sinh mL}$ (3.82)	$M \frac{(\cosh mL - \theta_L/\theta_b)}{\sinh mL}$ (3.83)
D	Infinite fin ($L \rightarrow \infty$): $\theta(L) = 0$	e^{-mx} (3.84)	M (3.85)

$\theta \equiv T - T_\infty$ $m^2 \equiv hP/kA_c$
 $\theta_b = \theta(0) = T_b - T_\infty$ $M \equiv \sqrt{hPkA_c} \theta_b$



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Transfert thermique et Echangeurs de chaleur & Phénomène de Transfert II

Module : **UEM1.1** Année : 21/20 Spécialité :Groupe : Durée : 60 min

Nom et prénom ::الاسم واللقب: Matricule:

Efficiency of common fin shapes

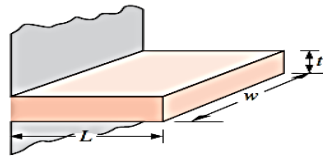
Straight Fins

Rectangular^a

$$A_f = 2wL_c$$

$$L_c = L + (t/2)$$

$$A_p = tL$$

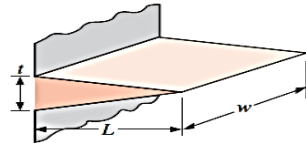


$$\eta_f = \frac{\tanh mL_c}{mL_c}$$

Triangular^a

$$A_f = 2w[L^2 + (t/2)^2]^{1/2}$$

$$A_p = (t/2)L$$



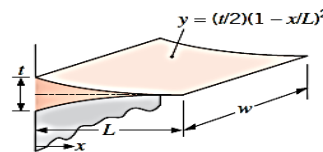
$$\eta_f = \frac{1}{mL} \frac{I_1(2mL)}{I_0(2mL)}$$

Parabolic^a

$$A_f = w[C_1L + (L^2/t)\ln(t/L + C_1)]$$

$$C_1 = [1 + (t/L)^2]^{1/2}$$

$$A_p = (t/3)L$$



$$\eta_f = \frac{2}{[4(mL)^2 + 1]^{1/2} + 1}$$

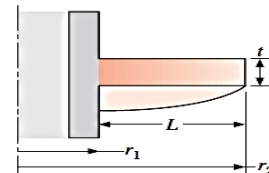
Circular Fin

Rectangular^a

$$A_f = 2\pi(r_{2c}^2 - r_1^2)$$

$$r_{2c} = r_2 + (t/2)$$

$$V = \pi(r_{2c}^2 - r_1^2)t$$



$$\eta_f = C_2 \frac{K_1(mr_1)I_1(mr_{2c}) - I_1(mr_1)K_1(mr_{2c})}{I_0(mr_1)K_1(mr_{2c}) + K_0(mr_1)I_1(mr_{2c})}$$

$$C_2 = \frac{(2r_1/m)}{(r_{2c}^2 - r_1^2)}$$

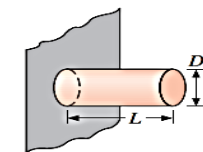
Pin Fins

Rectangular^b

$$A_f = \pi DL_c$$

$$L_c = L + (D/4)$$

$$V = (\pi D^2/4)L$$

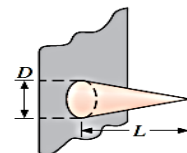


$$\eta_f = \frac{\tanh mL_c}{mL_c}$$

Triangular^b

$$A_f = \frac{\pi D}{2} [L^2 + (D/2)^2]^{1/2}$$

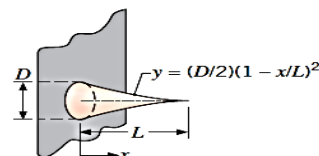
$$V = (\pi/12)D^2L$$



$$\eta_f = \frac{2}{mL} \frac{I_2(2mL)}{I_1(2mL)}$$

Parabolic^b

$$A_f = \frac{\pi L^3}{8D} \{ C_3 C_4 - \frac{L}{2D} \ln [(2DC_4/L) + C_3] \}$$



$$\eta_f = \frac{2}{[4/9(mL)^2 + 1]^{1/2} + 1}$$

$$C_3 = 1 + 2(D/L)^2$$

$$C_4 = [1 + (D/L)^2]^{1/2}$$

$$V = (\pi/20)D^2L$$

$$^a m = (2h/kt)^{1/2}$$

$$^b m = (4h/kD)^{1/2}$$



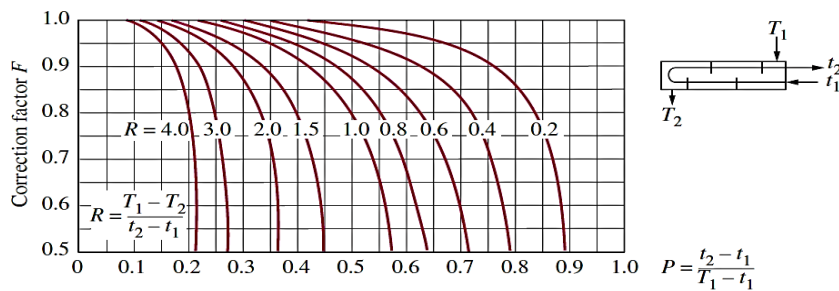
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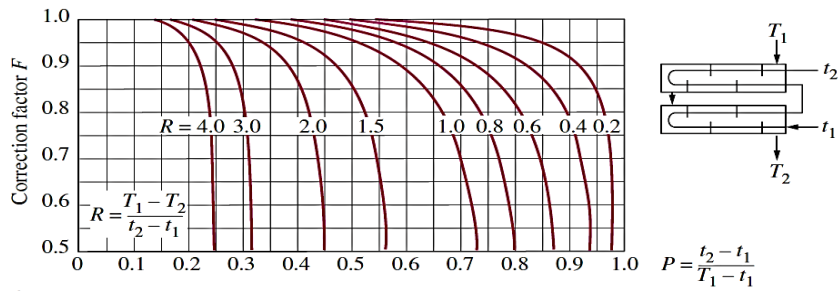
Module : **UEM1.1** Année : 21/20 Spécialité :Groupe : Durée : 60 min

Nom et prénom :: الاسم واللقب: Matricule:

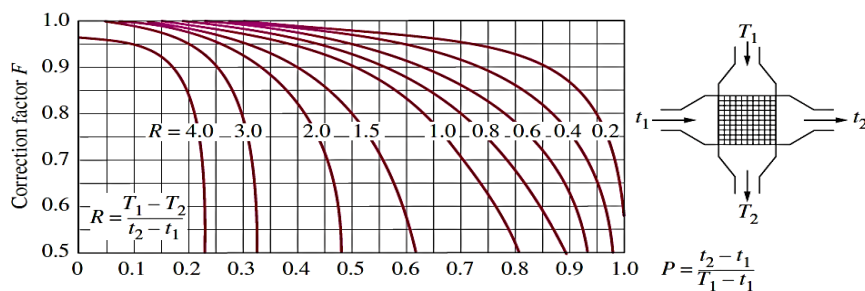
Diagrammes du facteur de correction F pour les échangeurs de chaleur à Faisceau et calandre (Shell and Tube) et à courant croisé (Cross-Flow).



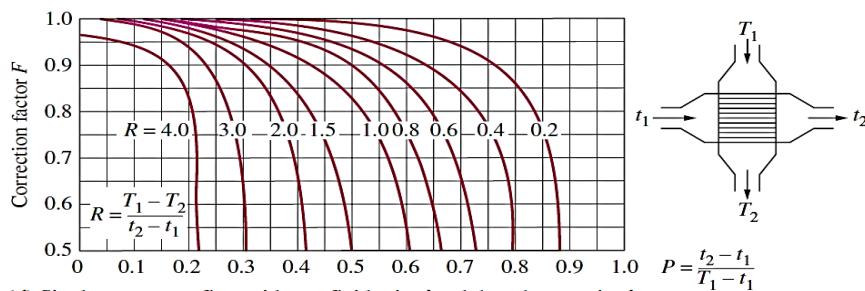
(a) One-shell pass and 2, 4, 6, etc. (any multiple of 2), tube passes



(b) Two-shell passes and 4, 8, 12, etc. (any multiple of 4), tube passes



(c) Single-pass cross-flow with both fluids unmixed



(d) Single-pass cross-flow with one fluid mixed and the other unmixed

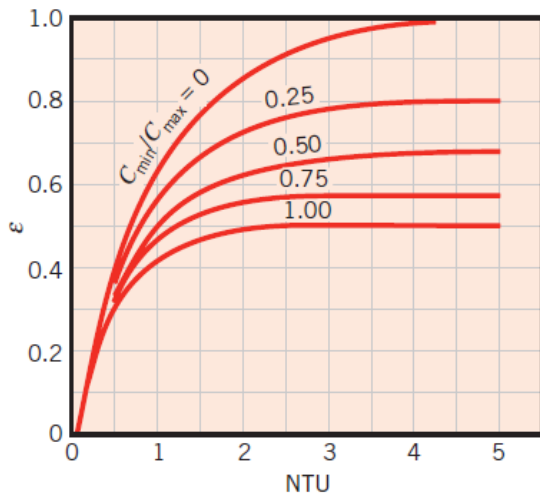


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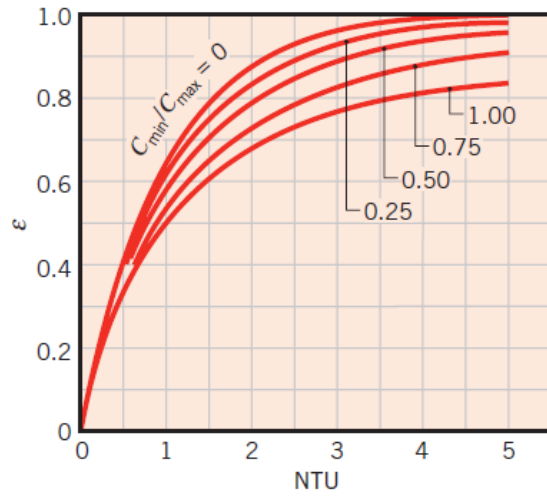
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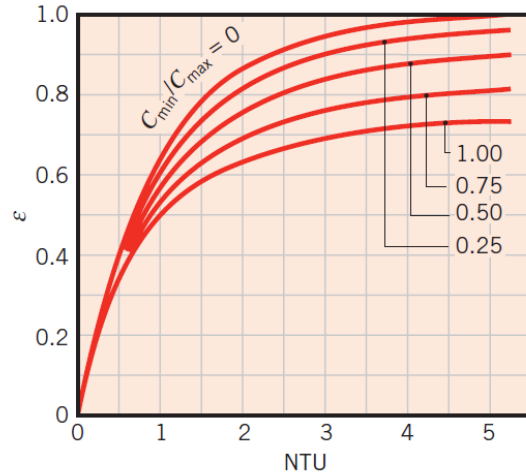
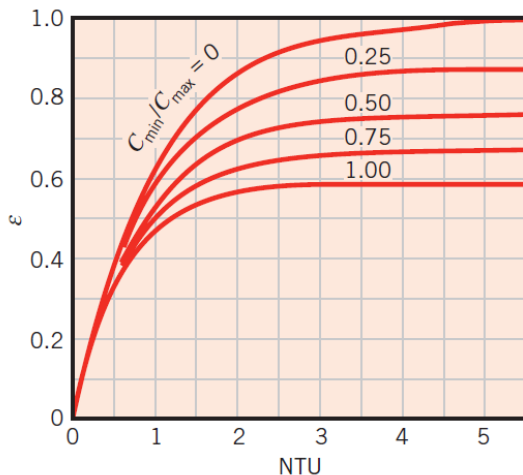
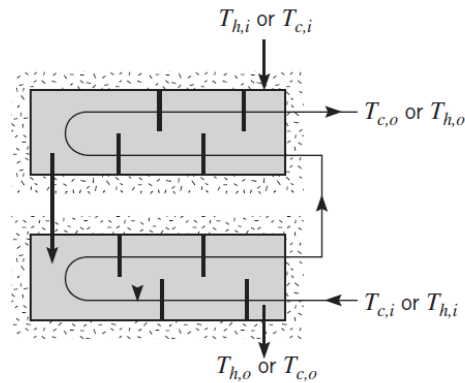
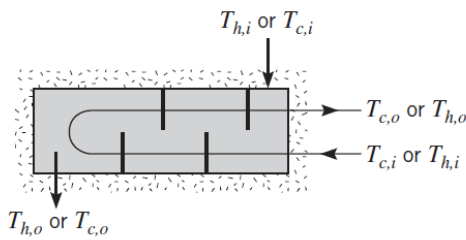
Abaques NUT = f(η) pour les échangeurs



Echangeur co-courant



Echangeur contre-courant





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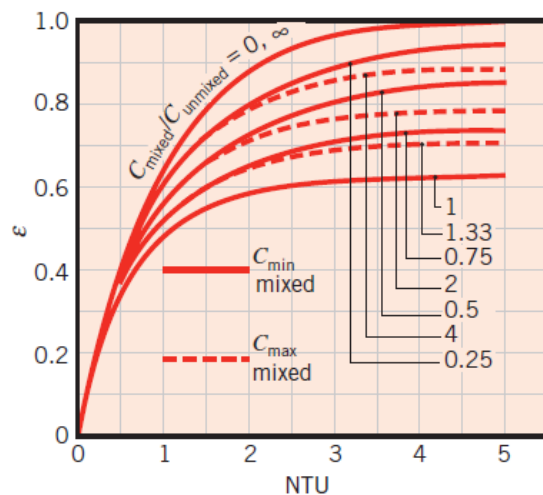
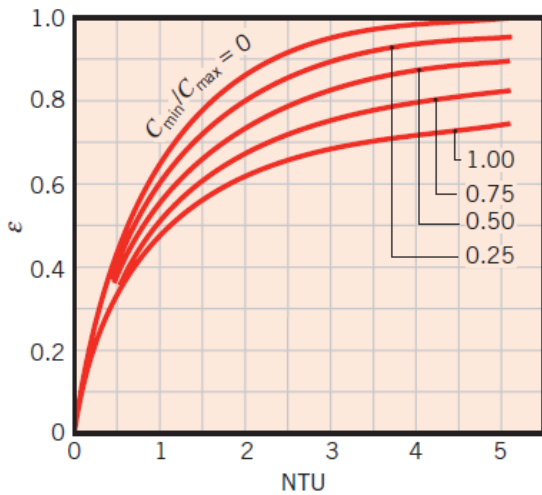
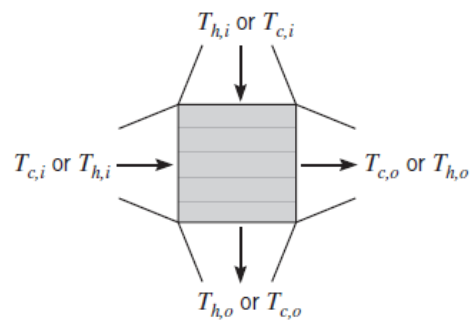
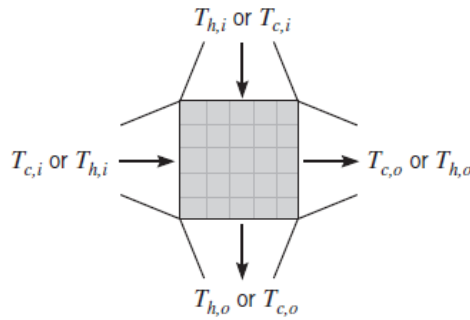
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Transfert thermique et Echangeurs de chaleur & Phénomène de Transfert II

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Abaques NUT = f(η) pour les échangeurs





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Flow Arrangement	Relation
Parallel flow	$\varepsilon = \frac{1 - \exp[-NTU(1 + C_r)]}{1 + C_r}$ (6.30.a)
Counterflow	$\varepsilon = \frac{1 - \exp[-NTU(1 - C_r)]}{1 - C_r \exp[-NTU(1 - C_r)]}$ ($C_r < 1$)
	$\varepsilon = \frac{NTU}{1 + NTU}$ ($C_r = 1$) (6.31.a)
Shell-and-tube	
One shell pass (2, 4, ... tube passes)	$\varepsilon_1 = 2 \left[1 + C_r + (1 + C_r^2)^{1/2} \times \frac{1 + \exp[-(NTU)_1(1 + C_r^2)^{1/2}]}{1 - \exp[-(NTU)_1(1 + C_r^2)^{1/2}]} \right]^{-1}$ (6.32.a)
n shell passes ($2n, 4n, \dots$ tube passes)	$\varepsilon = \left[\left(\frac{1 - \varepsilon_1 C_r}{1 - \varepsilon_1} \right)^n - 1 \right] \left[\left(\frac{1 - \varepsilon_1 C_r}{1 - \varepsilon_1} \right)^n - C_r \right]^{-1}$ (6.33.a)
Cross-flow (single pass)	
Both fluids unmixed	$\varepsilon = 1 - \exp \left[\left(\frac{1}{C_r} \right) (NTU)^{0.22} \{ \exp[-C_r(NTU)^{0.78}] - 1 \} \right]$ (6.34.a)
C_{\max} (mixed), C_{\min} (unmixed)	$\varepsilon = \left(\frac{1}{C_r} \right) (1 - \exp \{ -C_r [1 - \exp(-NTU)] \})$ (6.35.a)
C_{\min} (mixed), C_{\max} (unmixed)	$\varepsilon = 1 - \exp(-C_r^{-1} \{ 1 - \exp[-C_r(NTU)] \})$ (6.36.a)
All exchangers ($C_r = 0$)	$\varepsilon = 1 - \exp(-NTU)$ (6.37.a)

Flow Arrangement	Relation
Parallel flow	$NTU = -\frac{\ln[1 - \varepsilon(1 + C_r)]}{1 + C_r}$ (6.30.b)
Counterflow	$NTU = \frac{1}{C_r - 1} \ln \left(\frac{\varepsilon - 1}{\varepsilon C_r - 1} \right)$ ($C_r < 1$)
	$NTU = \frac{\varepsilon}{1 - \varepsilon}$ ($C_r = 1$) (6.31.b)
Shell-and-tube	
One shell pass (2, 4, ... tube passes)	$(NTU)_1 = -(1 + C_r^2)^{-1/2} \ln \left(\frac{E - 1}{E + 1} \right)$ $E = \frac{2\varepsilon_1 - (1 + C_r)}{(1 + C_r^2)^{1/2}}$ (6.32.b)
n shell passes ($2n, 4n, \dots$ tube passes)	Use Equations 11.30b and 11.30c with $\varepsilon_1 = \frac{F - 1}{F - C_r}$ $F = \left(\frac{\varepsilon C_r - 1}{\varepsilon - 1} \right)^{1/n}$ $NTU = n(NTU)_1$ (6.33.b)
Cross-flow (single pass)	
C_{\max} (mixed), C_{\min} (unmixed)	$NTU = -\ln \left[1 + \left(\frac{1}{C_r} \right) \ln(1 - \varepsilon C_r) \right]$ (6.34.b)
C_{\min} (mixed), C_{\max} (unmixed)	$NTU = -\left(\frac{1}{C_r} \right) \ln[C_r \ln(1 - \varepsilon) + 1]$ (6.35.b)
All exchangers ($C_r = 0$)	$NTU = -\ln(1 - \varepsilon)$ (6.36.b)



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Transfert thermique et Echangeurs de chaleur

Module : Année : 21/22 Spécialité : Groupe : Durée : .. min
Nom et prénom : الاسم واللقب : Matricule :

Properties of air at 1 atm pressure

Temp. $T, ^\circ\text{C}$	Density $\rho, \text{kg/m}^3$	Specific Heat $c_p, \text{J/kg}\cdot\text{K}$	Thermal Conductivity $k, \text{W/m}\cdot\text{K}$	Thermal Diffusivity $\alpha, \text{m}^2/\text{s}$	Dynamic Viscosity $\mu, \text{kg/m}\cdot\text{s}$	Kinematic Viscosity $\nu, \text{m}^2/\text{s}$	Prandtl Number Pr
-150	2.866	983	0.01171	4.158×10^{-6}	8.636×10^{-6}	3.013×10^{-6}	0.7246
-100	2.038	966	0.01582	8.036×10^{-6}	1.189×10^{-5}	5.837×10^{-6}	0.7263
-50	1.582	999	0.01979	1.252×10^{-5}	1.474×10^{-5}	9.319×10^{-6}	0.7440
-40	1.514	1002	0.02057	1.356×10^{-5}	1.527×10^{-5}	1.008×10^{-5}	0.7436
-30	1.451	1004	0.02134	1.465×10^{-5}	1.579×10^{-5}	1.087×10^{-5}	0.7425
-20	1.394	1005	0.02211	1.578×10^{-5}	1.630×10^{-5}	1.169×10^{-5}	0.7408
-10	1.341	1006	0.02288	1.696×10^{-5}	1.680×10^{-5}	1.252×10^{-5}	0.7387
0	1.292	1006	0.02364	1.818×10^{-5}	1.729×10^{-5}	1.338×10^{-5}	0.7362
5	1.269	1006	0.02401	1.880×10^{-5}	1.754×10^{-5}	1.382×10^{-5}	0.7350
10	1.246	1006	0.02439	1.944×10^{-5}	1.778×10^{-5}	1.426×10^{-5}	0.7336
15	1.225	1007	0.02476	2.009×10^{-5}	1.802×10^{-5}	1.470×10^{-5}	0.7323
20	1.204	1007	0.02514	2.074×10^{-5}	1.825×10^{-5}	1.516×10^{-5}	0.7309
25	1.184	1007	0.02551	2.141×10^{-5}	1.849×10^{-5}	1.562×10^{-5}	0.7296
30	1.164	1007	0.02588	2.208×10^{-5}	1.872×10^{-5}	1.608×10^{-5}	0.7282
35	1.145	1007	0.02625	2.277×10^{-5}	1.895×10^{-5}	1.655×10^{-5}	0.7268
40	1.127	1007	0.02662	2.346×10^{-5}	1.918×10^{-5}	1.702×10^{-5}	0.7255
45	1.109	1007	0.02699	2.416×10^{-5}	1.941×10^{-5}	1.750×10^{-5}	0.7241
50	1.092	1007	0.02735	2.487×10^{-5}	1.963×10^{-5}	1.798×10^{-5}	0.7228
60	1.059	1007	0.02808	2.632×10^{-5}	2.008×10^{-5}	1.896×10^{-5}	0.7202
70	1.028	1007	0.02881	2.780×10^{-5}	2.052×10^{-5}	1.995×10^{-5}	0.7177
80	0.9994	1008	0.02953	2.931×10^{-5}	2.096×10^{-5}	2.097×10^{-5}	0.7154
90	0.9718	1008	0.03024	3.086×10^{-5}	2.139×10^{-5}	2.201×10^{-5}	0.7132
100	0.9458	1009	0.03095	3.243×10^{-5}	2.181×10^{-5}	2.306×10^{-5}	0.7111
120	0.8977	1011	0.03235	3.565×10^{-5}	2.264×10^{-5}	2.522×10^{-5}	0.7073
140	0.8542	1013	0.03374	3.898×10^{-5}	2.345×10^{-5}	2.745×10^{-5}	0.7041
160	0.8148	1016	0.03511	4.241×10^{-5}	2.420×10^{-5}	2.975×10^{-5}	0.7014
180	0.7788	1019	0.03646	4.593×10^{-5}	2.504×10^{-5}	3.212×10^{-5}	0.6992
200	0.7459	1023	0.03779	4.954×10^{-5}	2.577×10^{-5}	3.455×10^{-5}	0.6974
250	0.6746	1033	0.04104	5.890×10^{-5}	2.760×10^{-5}	4.091×10^{-5}	0.6946
300	0.6158	1044	0.04418	6.871×10^{-5}	2.934×10^{-5}	4.765×10^{-5}	0.6935
350	0.5664	1056	0.04721	7.892×10^{-5}	3.101×10^{-5}	5.475×10^{-5}	0.6937
400	0.5243	1069	0.05015	8.951×10^{-5}	3.261×10^{-5}	6.219×10^{-5}	0.6948
450	0.4880	1081	0.05298	1.004×10^{-4}	3.415×10^{-5}	6.997×10^{-5}	0.6965
500	0.4565	1093	0.05572	1.117×10^{-4}	3.563×10^{-5}	7.806×10^{-5}	0.6986
600	0.4042	1115	0.06093	1.352×10^{-4}	3.846×10^{-5}	9.515×10^{-5}	0.7037
700	0.3627	1135	0.06581	1.598×10^{-4}	4.111×10^{-5}	1.133×10^{-4}	0.7092
800	0.3289	1153	0.07037	1.855×10^{-4}	4.362×10^{-5}	1.326×10^{-4}	0.7149
900	0.3008	1169	0.07465	2.122×10^{-4}	4.600×10^{-5}	1.529×10^{-4}	0.7206
1000	0.2772	1184	0.07868	2.398×10^{-4}	4.826×10^{-5}	1.741×10^{-4}	0.7260
1500	0.1990	1234	0.09599	3.908×10^{-4}	5.817×10^{-5}	2.922×10^{-4}	0.7478
2000	0.1553	1264	0.11113	5.664×10^{-4}	6.630×10^{-5}	4.270×10^{-4}	0.7539

Note: For ideal gases, the properties c_p , k , μ , and Pr are independent of pressure. The properties ρ , ν , and α at a pressure P (in atm) other than 1 atm are determined by multiplying the values of ρ at the given temperature by P and by dividing ν and α by P .



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Transfert thermique et Echangeurs de chaleur & Phénomène de Transfert II

Module : **UEM1.1** Année : 21/20 Spécialité :Groupe : Durée : 60 min

Nom et prénom :: الاسم واللقب: Matricule:

Saturated Liquids

T (K)	ρ (kg/m ³)	c_p (kJ/kg·K)	$\mu \cdot 10^2$ (N·s/m ²)	$\nu \cdot 10^6$ (m ² /s)	$k \cdot 10^3$ (W/m·K)	$\alpha \cdot 10^7$ (m ² /s)	Pr	$\beta \cdot 10^3$ (K ⁻¹)
Engine Oil (Unused)								
273	899.1	1.796	385	4280	147	0.910	47,000	0.70
280	895.3	1.827	217	2430	144	0.880	27,500	0.70
290	890.0	1.868	99.9	1120	145	0.872	12,900	0.70
300	884.1	1.909	48.6	550	145	0.859	6400	0.70
310	877.9	1.951	25.3	288	145	0.847	3400	0.70
320	871.8	1.993	14.1	161	143	0.823	1965	0.70
330	865.8	2.035	8.36	96.6	141	0.800	1205	0.70
340	859.9	2.076	5.31	61.7	139	0.779	793	0.70
350	853.9	2.118	3.56	41.7	138	0.763	546	0.70
360	847.8	2.161	2.52	29.7	138	0.753	395	0.70
370	841.8	2.206	1.86	22.0	137	0.738	300	0.70
380	836.0	2.250	1.41	16.9	136	0.723	233	0.70
390	830.6	2.294	1.10	13.3	135	0.709	187	0.70
400	825.1	2.337	0.874	10.6	134	0.695	152	0.70
410	818.9	2.381	0.698	8.52	133	0.682	125	0.70
420	812.1	2.427	0.564	6.94	133	0.675	103	0.70
430	806.5	2.471	0.470	5.83	132	0.662	88	0.70
Ethylene Glycol [C₂H₄(OH)₂]								
273	1130.8	2.294	6.51	57.6	242	0.933	617	0.65
280	1125.8	2.323	4.20	37.3	244	0.933	400	0.65
290	1118.8	2.368	2.47	22.1	248	0.936	236	0.65
300	1114.4	2.415	1.57	14.1	252	0.939	151	0.65
310	1103.7	2.460	1.07	9.65	255	0.939	103	0.65
320	1096.2	2.505	0.757	6.91	258	0.940	73.5	0.65
330	1089.5	2.549	0.561	5.15	260	0.936	55.0	0.65
340	1083.8	2.592	0.431	3.98	261	0.929	42.8	0.65
350	1079.0	2.637	0.342	3.17	261	0.917	34.6	0.65
360	1074.0	2.682	0.278	2.59	261	0.906	28.6	0.65
370	1066.7	2.728	0.228	2.14	262	0.900	23.7	0.65
373	1058.5	2.742	0.215	2.03	263	0.906	22.4	0.65
Glycerin [C₃H₅(OH)₃]								
273	1276.0	2.261	1060	8310	282	0.977	85,000	0.47
280	1271.9	2.298	534	4200	284	0.972	43,200	0.47
290	1265.8	2.367	185	1460	286	0.955	15,300	0.48
300	1259.9	2.427	79.9	634	286	0.935	6780	0.48
310	1253.9	2.490	35.2	281	286	0.916	3060	0.49
320	1247.2	2.564	21.0	168	287	0.897	1870	0.50



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Transfert thermique et Echangeurs de chaleur & Phénomène de Transfert II

Module : **UEM1.1** Année : 21/20 Spécialité :Groupe : Durée : 60 min

Nom et prénom ::الاسم واللقب:..... Matricule:.....

Thermophysical Properties of Saturated Water^a

Temperature, T (K)	Pressure, p (bars) ^b	Specific Volume (m ³ /kg)		Heat of Vaporization, h_{fg} (kJ/kg)	Specific Heat (kJ/kg · K)		Viscosity (N · s/m ²)		Thermal Conductivity (W/m · K)		Prandtl Number		Surface Tension, $\sigma_f \cdot 10^3$ (N/m)	Expansion Coefficient, $\beta_f \cdot 10^6$ (K ⁻¹)	Temperature, T (K)
		$v_f \cdot 10^3$	v_g		$c_{p,f}$	$c_{p,g}$	$\mu_f \cdot 10^6$	$\mu_g \cdot 10^6$	$k_f \cdot 10^3$	$k_g \cdot 10^3$	Pr_f	Pr_g			
273.15	0.00611	1.000	206.3	2502	4.217	1.854	1750	8.02	569	18.2	12.99	0.815	75.5	-68.05	273.15
275	0.00697	1.000	181.7	2497	4.211	1.855	1652	8.09	574	18.3	12.22	0.817	75.3	-32.74	275
280	0.00990	1.000	130.4	2485	4.198	1.858	1422	8.29	582	18.6	10.26	0.825	74.8	46.04	280
285	0.01387	1.000	99.4	2473	4.189	1.861	1225	8.49	590	18.9	8.81	0.833	74.3	114.1	285
290	0.01917	1.001	69.7	2461	4.184	1.864	1080	8.69	598	19.3	7.56	0.841	73.7	174.0	290
295	0.02617	1.002	51.94	2449	4.181	1.868	959	8.89	606	19.5	6.62	0.849	72.7	227.5	295
300	0.03531	1.003	39.13	2438	4.179	1.872	855	9.09	613	19.6	5.83	0.857	71.7	276.1	300
305	0.04712	1.005	29.74	2426	4.178	1.877	769	9.29	620	20.1	5.20	0.865	70.9	320.6	305
310	0.06221	1.007	22.93	2414	4.178	1.882	695	9.49	628	20.4	4.62	0.873	70.0	361.9	310
315	0.08132	1.009	17.82	2402	4.179	1.888	631	9.69	634	20.7	4.16	0.883	69.2	400.4	315
320	0.1053	1.011	13.98	2390	4.180	1.895	577	9.89	640	21.0	3.77	0.894	68.3	436.7	320
325	0.1351	1.013	11.06	2378	4.182	1.903	528	10.09	645	21.3	3.42	0.901	67.5	471.2	325
330	0.1719	1.016	8.82	2366	4.184	1.911	489	10.29	650	21.7	3.15	0.908	66.6	504.0	330
335	0.2167	1.018	7.09	2354	4.186	1.920	453	10.49	656	22.0	2.88	0.916	65.8	535.5	335
340	0.2713	1.021	5.74	2342	4.188	1.930	420	10.69	660	22.3	2.66	0.925	64.9	566.0	340
345	0.3372	1.024	4.683	2329	4.191	1.941	389	10.89	664	22.6	2.45	0.933	64.1	595.4	345
350	0.4163	1.027	3.846	2317	4.195	1.954	365	11.09	668	23.0	2.29	0.942	63.2	624.2	350
355	0.5100	1.030	3.180	2304	4.199	1.968	343	11.29	671	23.3	2.14	0.951	62.3	652.3	355
360	0.6209	1.034	2.645	2291	4.203	1.983	324	11.49	674	23.7	2.02	0.960	61.4	679.9	360
365	0.7514	1.038	2.212	2278	4.209	1.999	306	11.69	677	24.1	1.91	0.969	60.5	707.1	365
370	0.9040	1.041	1.861	2265	4.214	2.017	289	11.89	679	24.5	1.80	0.978	59.5	728.7	370
373.15	1.0133	1.044	1.679	2257	4.217	2.029	279	12.02	680	24.8	1.76	0.984	58.9	750.1	373.15
375	1.0815	1.045	1.574	2252	4.220	2.036	274	12.09	681	24.9	1.70	0.987	58.6	761	375
380	1.2869	1.049	1.337	2239	4.226	2.057	260	12.29	683	25.4	1.61	0.999	57.6	788	380
385	1.5233	1.053	1.142	2225	4.232	2.080	248	12.49	685	25.8	1.53	1.004	56.6	814	385
390	1.794	1.058	0.980	2212	4.239	2.104	237	12.69	686	26.3	1.47	1.013	55.6	841	390
400	2.455	1.067	0.731	2183	4.256	2.158	217	13.05	688	27.2	1.34	1.033	53.6	896	400
410	3.302	1.077	0.553	2153	4.278	2.221	200	13.42	688	28.2	1.24	1.054	51.5	952	410
420	4.370	1.088	0.425	2123	4.302	2.291	185	13.79	688	29.8	1.16	1.075	49.4	1010	420
430	5.699	1.099	0.331	2091	4.331	2.369	173	14.14	685	30.4	1.09	1.10	47.2		430



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Transfert thermique et Echangeurs de chaleur & Phénomène de Transfert II

Module : **UEM1.1** Année : 21/20 Spécialité :Groupe : Durée : 60 min

Nom et prénom ::الاسم واللقب:..... Matricule:.....

Continued

Temperature, T (K)	Pressure, p (bars) ^b	Specific Volume (m ³ /kg)		Heat of Vaporization, h_{fg} (kJ/kg)	Specific Heat (kJ/kg · K)		Viscosity (N · s/m ²)		Thermal Conductivity (W/m · K)		Prandtl Number		Surface Tension, $\sigma_f \cdot 10^3$ (N/m)	Expansion Coefficient, $\beta_f \cdot 10^6$ (K ⁻¹)	Temperature, T (K)
		$v_f \cdot 10^3$	v_g		$c_{p,f}$	$c_{p,g}$	$\mu_f \cdot 10^6$	$\mu_g \cdot 10^6$	$k_f \cdot 10^3$	$k_g \cdot 10^3$	Pr_f	Pr_g			
440	7.333	1.110	0.261	2059	4.36	2.46	162	14.50	682	31.7	1.04	1.12	45.1	—	440
450	9.319	1.123	0.208	2024	4.40	2.56	152	14.85	678	33.1	0.99	1.14	42.9	—	450
460	11.71	1.137	0.167	1989	4.44	2.68	143	15.19	673	34.6	0.95	1.17	40.7	—	460
470	14.55	1.152	0.136	1951	4.48	2.79	136	15.54	667	36.3	0.92	1.20	38.5	—	470
480	17.90	1.167	0.111	1912	4.53	2.94	129	15.88	660	38.1	0.89	1.23	36.2	—	480
490	21.83	1.184	0.0922	1870	4.59	3.10	124	16.23	651	40.1	0.87	1.25	33.9	—	490
500	26.40	1.203	0.0766	1825	4.66	3.27	118	16.59	642	42.3	0.86	1.28	31.6	—	500
510	31.66	1.222	0.0631	1779	4.74	3.47	113	16.95	631	44.7	0.85	1.31	29.3	—	510
520	37.70	1.244	0.0525	1730	4.84	3.70	108	17.33	621	47.5	0.84	1.35	26.9	—	520
530	44.58	1.268	0.0445	1679	4.95	3.96	104	17.72	608	50.6	0.85	1.39	24.5	—	530
540	52.38	1.294	0.0375	1622	5.08	4.27	101	18.1	594	54.0	0.86	1.43	22.1	—	540
550	61.19	1.323	0.0317	1564	5.24	4.64	97	18.6	580	58.3	0.87	1.47	19.7	—	550
560	71.08	1.355	0.0269	1499	5.43	5.09	94	19.1	563	63.7	0.90	1.52	17.3	—	560
570	82.16	1.392	0.0228	1429	5.68	5.67	91	19.7	548	76.7	0.94	1.59	15.0	—	570
580	94.51	1.433	0.0193	1353	6.00	6.40	88	20.4	528	76.7	0.99	1.68	12.8	—	580
590	108.3	1.482	0.0163	1274	6.41	7.35	84	21.5	513	84.1	1.05	1.84	10.5	—	590
600	123.5	1.541	0.0137	1176	7.00	8.75	81	22.7	497	92.9	1.14	2.15	8.4	—	600
610	137.3	1.612	0.0115	1068	7.85	11.1	77	24.1	467	103	1.30	2.60	6.3	—	610
620	159.1	1.705	0.0094	941	9.35	15.4	72	25.9	444	114	1.52	3.46	4.5	—	620
625	169.1	1.778	0.0085	858	10.6	18.3	70	27.0	430	121	1.65	4.20	3.5	—	625
630	179.7	1.856	0.0075	781	12.6	22.1	67	28.0	412	130	2.0	4.8	2.6	—	630
635	190.9	1.935	0.0066	683	16.4	27.6	64	30.0	392	141	2.7	6.0	1.5	—	635
640	202.7	2.075	0.0057	560	26	42	59	32.0	367	155	4.2	9.6	0.8	—	640
645	215.2	2.351	0.0045	361	90	—	54	37.0	331	178	12	26	0.1	—	645
647.3 ^c	221.2	3.170	0.0032	0	∞	∞	45	45.0	238	238	∞	∞	0.0	—	647.3 ^c

^aAdapted from Reference 22.

^b1 bar = 10⁵ N/m².

^cCritical temperature.



الجمهورية الجزائرية الديمقراطية الشعبية
وزارة التعليم العالي والبحث العلمي
جامعة الشهيد حمه لخضر الوادي
كلية التكنولوجيا
قسم هندسة الطرائق والصناعات البتر وكيميائية
Document autorisé



Transfert thermique et Echangeurs de chaleur & Phénomène de Transfert II

Module : **UEM1.1** Année : 21/20 Spécialité :Groupe : Durée : 60 min

Nom et prénom ::الاسم واللقب:..... Matricule:.....

Useful conversion factors

Physical quantity	Symbol	SI to English conversion	English to SI conversion
Length	L	1 m = 3.2808 ft	1 ft = 0.3048 m
Area	A	1 m ² = 10.7639 ft ²	1 ft ² = 0.092903 m ²
Volume	V	1 m ³ = 35.3134 ft ³	1 ft ³ = 0.028317 m ³
Velocity	v	1 m/s = 3.2808 ft/s	1 ft/s = 0.3048 m/s
Density	ρ	1 kg/m ³ = 0.06243 lb _m /ft ³	1 lb _m /ft ³ = 16.018 kg/m ³
Force	F	1 N = 0.2248 lb _f	1 lb _f = 4.4482 N
Mass	m	1 kg = 2.20462 lb _m	1 lb _m = 0.45359237 kg
Pressure	p	1 N/m ² = 1.45038 × 10 ⁻⁴ lb _f /in ²	1 lb _f /in ² = 6894.76 N/m ²
Energy, heat	q	1 kJ = 0.94783 Btu	1 Btu = 1.05504 kJ
Heat flow	q	1 W = 3.4121 Btu/h	1 Btu/h = 0.29307 W
Heat flux per unit area	q/A	1 W/m ² = 0.317 Btu/h · ft ²	1 Btu/h · ft ² = 3.154 W/m ²
Heat flux per unit length	q/L	1 W/m = 1.0403 Btu/h · ft	1 Btu/h · ft = 0.9613 W/m
Heat generation per unit volume	\dot{q}	1 W/m ³ = 0.096623 Btu/h · ft ³	1 Btu/h · ft ³ = 10.35 W/m ³
Energy per unit mass	q/m	1 kJ/kg = 0.4299 Btu/lb _m	1 Btu/lb _m = 2.326 kJ/kg
Specific heat	c	1 kJ/kg · °C = 0.23884 Btu/lb _m · °F	1 Btu/lb _m · °F = 4.1869 kJ/kg · °C
Thermal conductivity	k	1 W/m · °C = 0.5778 Btu/h · ft · °F	1 Btu/h · ft · °F = 1.7307 W/m · °C
Convection heat-transfer coefficient	h	1 W/m ² · °C = 0.1761 Btu/h · ft ² · °F	1 Btu/h · ft ² · °F = 5.6782 W/m ² · °C
Dynamic		1 kg/m · s = 0.672 lb _m /ft · s	
Viscosity	μ	= 2419.2 lb _m /ft · h	1 lb _m /ft · s = 1.4881 kg/m · s
Kinematic viscosity and thermal diffusivity	ν, α	1 m ² /s = 10.7639 ft ² /s	1 ft ² /s = 0.092903 m ² /s

Important physical constants

Avogadro's number	$N_0 = 6.022045 \times 10^{26}$ molecules/kg mol
Universal gas constant	$R = 1545.35$ ft · lb _f /lb _m · mol · °R = 8314.41 J/kg mol · K = 1.986 Btu/lb _m · mol · °R = 1.986 kcal/kg mol · K
Planck's constant	$h = 6.626176 \times 10^{-34}$ J · sec
Boltzmann's constant	$k = 1.380662 \times 10^{-23}$ J/molecule · K = 8.6173 × 10 ⁻⁵ eV/molecule · K
Speed of light in vacuum	$c = 2.997925 \times 10^8$ m/s
Standard gravitational acceleration	$g = 32.174$ ft/s ² = 9.80665 m/s ²
Electron mass	$m_e = 9.1095 \times 10^{-31}$ kg
Charge on the electron	$e = 1.602189 \times 10^{-19}$ C
Stefan-Boltzmann constant	$\sigma = 0.1714 \times 10^{-8}$ Btu/hr · ft ² · R ⁴ = 5.669 × 10 ⁻⁸ W/m ² · K ⁴
1 atm	= 14.69595 lb _f /in ² = 760 mmHg at 32°F = 29.92 inHg at 32°F = 2116.21 lb _f /ft ² = 1.01325 × 10 ⁵ N/m ²